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# Appliances Modeling And Simulation: A Virtual Platform Applied For Arc Fault Testing

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**Abstract**—This study is devoted to the development of a virtual electric network composed by linear and nonlinear household appliances, the supply voltage and an arc fault which can be inserted in series or in parallel in the line. The configuration and composition of the entire device can be changed at will. This virtual platform is used to the establishment of a current and line voltage signatures database for the development of an arc fault detector. We describe in this paper some load modeling using both Matlab/simulink (for the performed universal motor model) and SimPowerSystem block (for the supply voltage, wires and arc models). The simulation platform presented includes a vacuum cleaner, a discharge lamp, a drill and an electric arc fault. Validation criteria of the different models are based on the comparison of the harmonic distortion (frequency characteristic) and the calculus of the index of agreement (time characteristic). The experimental results obtained validate the models for single and combined loads in the presence or not of an arc in series in the electric line.

**Index Terms**—modelling, domestic loads, arc fault, detection

## I. INTRODUCTION

An electrical arc fault particularly in a domestic installation is a dangerous phenomenon that may cause fire ignitions. In 2010, an estimation of 46500 fires in the home structures [1] caused by an apparatus malfunction or electrical failure (mainly by over-current, short-circuit, insulation fault or worst contact) have been reported. The development of arc faults detectors [2] [3] based mostly on the electrical current and line voltage signatures requires a large signals database reproducing many different situations according to the number and type of loads on the network (single loads, combined loads, parallel and series arc.).

In order to get away from an experimental phase, which can often be complicated to set up, we opted for an approach based on the development of a configurable virtual domestic network which operates closest to the reality.

The choice of simulation software to develop the entire virtual network is essential. Although all the domestic network loads are electrical ones (including power devices), others may require the modeling of electromechanical and mechanical devices. The software platform should also allow the simulation of both the numerical detection system and our home network model [4]. All simulations are performed with MatLab/Simulink - SimPowerSystem software.

On the same, loads modeled with other software (Pspice, Psim ....) can be easily integrated in the virtual network.

Fig. 1 shows the general diagram of the power line model. It contains a power supply (230 VAC -50 Hz), a circuit breaker, the electrical wires and also the different domestic loads (simple or combined associations). The electrical arcing fault occurs either in serial or in parallel mode. The circuit breaker which analyzes the current and voltage on the line is located upstream of the line to be protected, but will not be modeled in this study.

The main objective is to get the electrical signatures (line current and voltage) unique and specific to each device and to build a complete database.

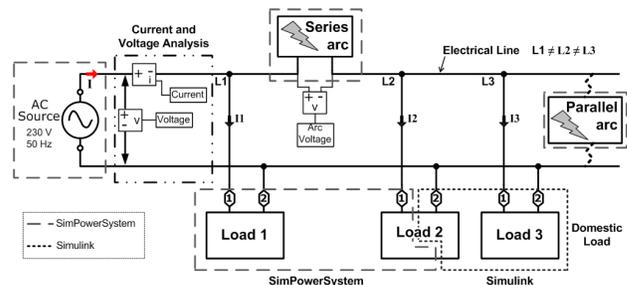


Fig. 1: Electrical network model including models of arc fault on Simulink.

In the literature, main modellings concern linear and nonlinear loads largely used for domestic application. Several models of domestic and industrial loads have been developed such as personal computers [5] [6], fluorescent lamp [5], adjustable speed drives [5]. Modeling presented in this work will principally focus on a vacuum cleaner and the drill with an improved electric motor model. In literature, Di Gerlando et al. [7] [8] propose a transient model of a universal motor model by modeling the influences of the saturation inductances and taking into account the constructional quantities of the machine. Tuncay [9] present a universal motor model for a vacuum cleaner. In our work, we favored a modelling of the DC engine which not require the knowledge of all the parameters necessary for the previous models. The modelling is based on the electric and mechanical equations of the engine. The modelling of the drill as well as the vacuum

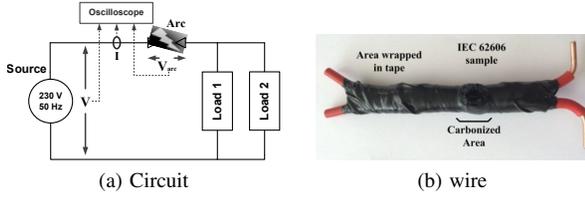


Fig. 2: Experimental test

cleaner is obtained by adding the modules of torque functions and power variation appropriate to every device to obtain the current line signature the closest to the reality.

The results of current and voltage are obtained experimentally with simple load and also with combined loads. Moreover, these two configurations are reproduced with a series arc fault on the line. For each test, we compare experimental and simulate results using the total harmonic distortion THD (frequency characteristic) and the index of agreement (time characteristic).

## II. TEST SET UP AND MODELS VALIDATION

In order to evaluate the performance of the model, simulated and measured current signatures are compared both by harmonic analysis (total harmonic distortion- THD) and shape analysis (index of agreement).

### A. Models validation

The THD is defined as the ratio of the rms value of the total harmonics to the rms value of the fundamental component according to equation (1):

$$THD\% = \frac{\sqrt{\sum_{n=2,3,4}^{20} h_n^2}}{h_1} * 100\% \quad (1)$$

The index of agreement (d) [10] is estimated according to (2) from the simulated value P, the observed value O and the observed mean value  $\bar{O}$ .

$$d = 1 - \frac{\sum_{i=1}^k (O_i - P_i)^2}{\sum_{i=1}^k (|P_i - \bar{O}| + |O_i - \bar{O}|)^2} \quad (2)$$

### B. Experimental test set up

Fig. 2 shows the schematic configuration of experimental system (arc fault generation and data acquisition). A series arc fault is generated using carbonized path [11] [12] [13] between two domestic copper wires [11], the circuit is powered with 230 VAC / 50 Hz.

The characteristics of the current and voltage probes are given in the table I. Data acquisition is carried out by a Lecroy oscilloscope wavepro 950 (1 GHz).

TABLE I: Current and Voltage characteristics

Load	Voltage	Current
Model	Lecroy PPe 20 kV	Lecroy AP015
Bandwidth	DC - 100 MHz	DC - 50 MHz
Max. peak	20 kV	50 A

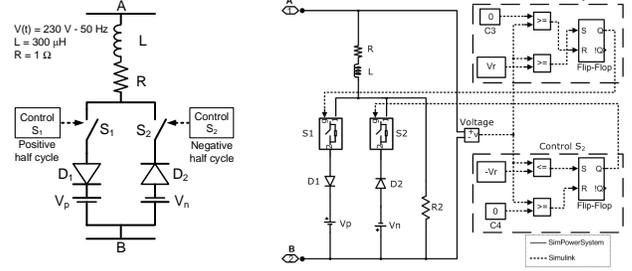


Fig. 3: Electrical model and simulation diagram of an arc fault.

## III. ARC FAULT MODELING

Many authors have proposed models to describe an arcing fault. Emanuel et al. [14] as for them proposed a model with two DC sources connected in opposite direction by means of two diodes and two voltage sources representing the arc voltage. Etemadi et al. [15] uses the same model and adds two resistances,  $R_p$  and  $R_n$  which represent the fault resistance. Based on the other models, Zamanan et al. [16] [17] proposed a dynamic by adding two inductances  $L_p$  and  $L_n$  which introduce nonlinearity in the V-I curve. Sedighi et al. [18] used combinations of nonlinear varying resistor and also introduced a switch controlling the loop opening and closing. Our model based on the Zamanans one [16] [17] and Andrea [19], comprises a switch control to generate the arc restrike voltage. When the line voltage reached the restrike voltage ( $V_r$ ), the switch is closed so the current flows across the arc circuit. Restrike voltage  $V_r$  can be set differently depending on the positive or negative half cycle. The arc voltage reaches  $V_p$  or  $V_n$ . The switch S is opened at each zero crossing. Fig. 3 shows the block diagram of the arc fault and model implemented with Matlab Simulink / SimPowerSystem.

The values of the parameters used for modeling. Diodes are considered ideal.  $V_r=60$  V,  $V_p = V_n = 25$  V,  $R= 4 \Omega$  and  $L = 400 \mu H$ .

The comparison of measured and modeled current curves is presented on Fig. 4. The two currents signatures present a great similarity ( $d=98.03\%$ ). Some differences appear especially at the arc ignition.

The results show that the harmonic content of the measured and modeled signals are of the same order (THD meas = 30.06% and THD model = 38.32%).

In both cases, the harmonics amplitude of order 1, 3 and 5 prevails. The values given by the modelling are however superior to the values measured for all the odd orders. These differences are mainly related to symmetry of the arc signal

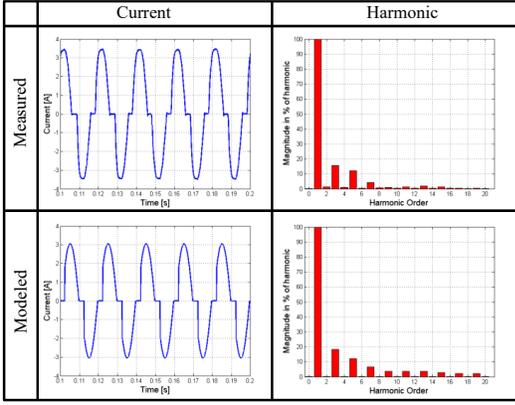


Fig. 4: Current arc fault signatures.

in the model while it is not completely the case in the reality. Furthermore, the arc signal is widely chaotic in time, its physical characteristics being modified from one period to the other one, phenomenon which is not taken into account in the model.

The harmonics amplitudes of even order are very low as well for the measured signal and the modelled one. In the modelling, the signal of current being perfectly symmetric, the even harmonics are equal to zero.

#### IV. DOMESTIC LOAD MODELING

We have used the classification of all domestic loads proposed by Ting et al. [20] based on four types of loads (resistive, inductive, rectified load and motor) as shown in Fig. 5.

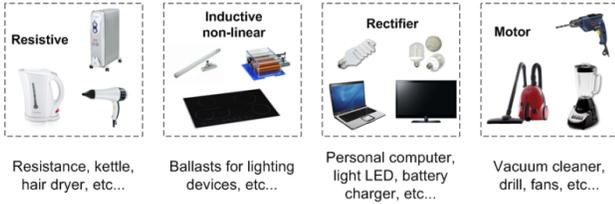


Fig. 5: Load Signature classification.

Resistive loads (kettle, hair dryer, ...) relatively simple to be modeled will not be taken into account in this work. This is also the case of rectifier type loads, usually equipped with power factor corrector module. Among the inductive / non-linear loads, we present the model of the domestic appliances based on a universal motor will also be developed.

##### A. Universal motor model

1) *Electrical and mechanical part modeling*: Universal motor is widely used in many domestic appliances (washing machine, mixer, blender, drill). It can operate with a single AC supplies and also with DC supplies. In the universal motor, the stator and rotor windings are connected in series [7] [8] [21]. The model we propose added the torque functions and power variation. These functions allow us to take into account the variation of current due to fluctuations of torque

electromagnetic and also the current evolution. Fig. 6 shows the blocks diagram of the universal motor which is described traditionally by three equations: electrical part (3), mechanical part (4) and load torque.

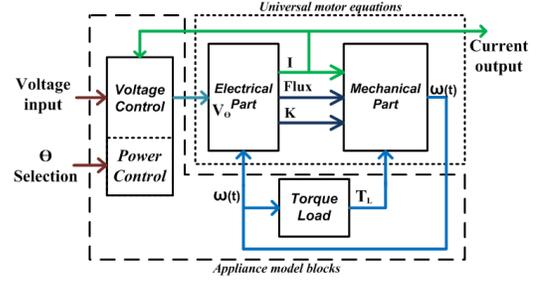


Fig. 6: Diagram for appliance using a universal motor.

- The electrical part

$$u(t) - (L_a + L_f) \frac{d}{dt} i(t) - e(t) = (R_a + R_f) i(t) \quad (3)$$

- The mechanical part

$$T_e(t) = T_L + D * w_m + J \frac{d}{dt} w_m \quad (4)$$

Where:  $R_a$  is the rotor winding resistance.  $R_f$  is the stator winding resistance.  $L_a$  is the rotor winding inductance.  $L_f$  is the stator winding inductance.  $u(t)$  is the input voltage.  $e(t)$  is the electromotive force.  $i(t)$  is the current.  $J$  is the moment of inertia.  $D$  is the viscous damping constant.  $T_e(t)$  is the electromagnetic torque.  $T_L$  is the load torque.  $w_m(t)$  is the angular velocity.

Fig. 7 shows the electrical modeling of the motor inserted on the line. The appliance is modeled using matlab simulink and the electrical network by SimPowerSystem.

The general supply voltage and the propagation line being modelled under SimpowerSystem, a load modeled in Simulink can not be directly inserted into the resulting network. It is thus necessary to inject the consumption current of every load in the general electric line by a controlled current source connected in close loop. "This will have for consequence that any disturbance related in particular to a defect of electric arc which can occur upstream to the load is going to be injected on the entrance of this one through the current and the voltage of line".

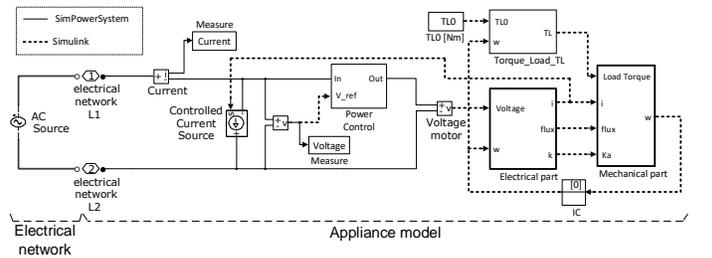


Fig. 7: Appliance model in Matlab Simulink

## V. RESULTS

### A. Drill with an Arc Fault

In this test an arc fault in series with a drill is presented (Fig. 8)

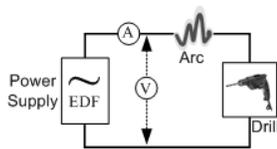


Fig. 8: Drill in series with an arc fault.

Fig. 9 shows the measured and simulated current, harmonic analysis and the validation criteria values.

Fig. 10 shows a good agreement between the current experimental and the current measured,  $d$  reaches 97.73%.

The presence in the model of a zero crossing current can explain the relatively important difference of the 3 order harmonic amplitude between the model and the measurement. The difference between amplitude of odd harmonics (THD meas = 24.79 %, THD model 15.75 %) can be related to the fact that several parameters such as switching of the collector's for the drill model and spark effect in the arc fault model are not taken into account in the modelling. Furthermore, the modelled current is perfectly symmetric and doesn't contain any offset voltage.

The global THD values for measured and simulated currents have a difference of about 7%, (TDH meas = 25.01% TDH model = 15.76%) due to parameters described before. The amplitudes of even harmonics are close to zero for the whole orders. The presence of an offset voltage on the probe is translated by a rather strong value of the continuous component.

### B. Masking Load

Masking load consists in two or more loads connected in parallel, wherein a series arcing fault occurs in the circuit. This test is composed by a vacuum cleaner in parallel with a radiator in series with an arc fault (Fig. 11).

TABLE II: Simulation parameters of Fig. 11.

Simulation parameters	
Voltage	120 V / 50 Hz
Vaccum cleaner	Power 750 W Load torque 0.5 Nm Phase control 60°
Resistance	$R = 11 \Omega$

Fig. 12 shows the results both for simulation and modeling. The good index of agreement (99.7 %) shows the great similarity between simulated and measured current waveform

By taking into account three different loads on the line, the total distortion harmonic global in both cases is similar (THD meas = 15.29 % THD model = 16.75 %). The most pronounced difference concerns the 7 and 9 harmonics order

to a lesser extent. For odd harmonics, the rates of distortions remain however rather close (THD odd meas = 15.18%, THD odd model 16.75 %). These variations are due to some parameters from load model (motor torque and line voltage variation) and arc model that are not taken into account. For the even harmonics, the values are very low in both cases (THD even meas = 1.82 %, THD even model 0.23 %).

## VI. CONCLUSIONS

In this paper, a simulation platform has been presented in order to recreate a virtual domestic electrical installation. This platform is an essential tool for the development and testing, in a reliable way, of arc fault detection methods based on the supervision of the current and voltage on the electric line. THD estimation and index of agreement value are two pertinent indicators allowing to compare current signatures from modeling and measurement.

In order to model a drill and a vacuum cleaner, we took back the equations of the literature describing the electric and mechanical part of a universal motor to which we added the power and torque regulation modulus. We showed that it was possible to develop the different domestic load models using both MatLab Simulink and SimPowerSystem. All simulink/SPS models are presented in details and compared with experimental measurements.

A good concordance in the calculation of the total harmonic distortion and a value of the index of agreement upper to 0.95 shows also that simulated curves are in good concordance with experimental ones. The good agreement between experimental and modeled results concern both the case of single and combined loads. The results showed the possibility to build many different configurations of the electric network by varying the number and type of loads. Furthermore, an arcing fault model can be inserted anywhere in the electric line.

The future works will concern the development of simulation models of other types of loads (PC compute, television) to complete the database for domestic installation modeling including the presence of an arc fault in the circuit.

## ACKNOWLEDGMENT

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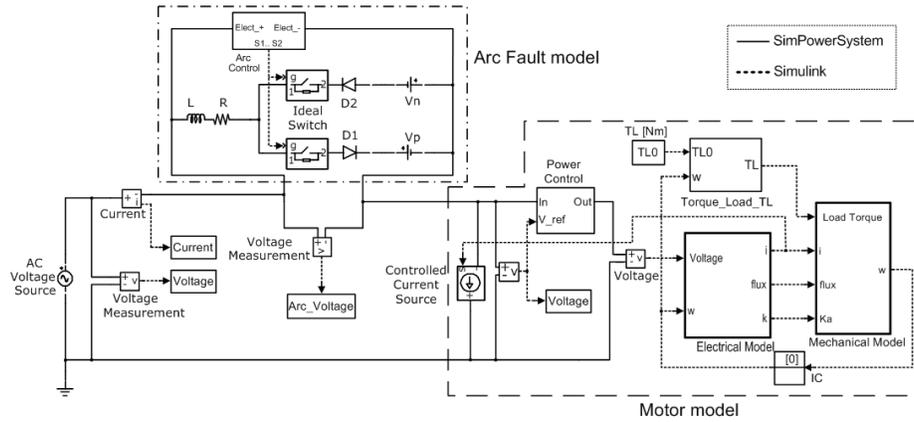


Fig. 9: Drill in series with an arc fault model.

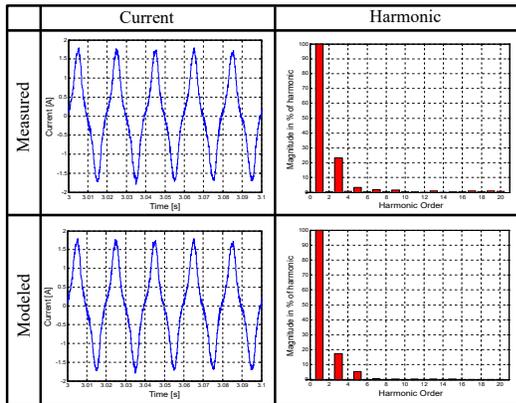


Fig. 10: Measured and simulated current for an arc fault in series with a drill.

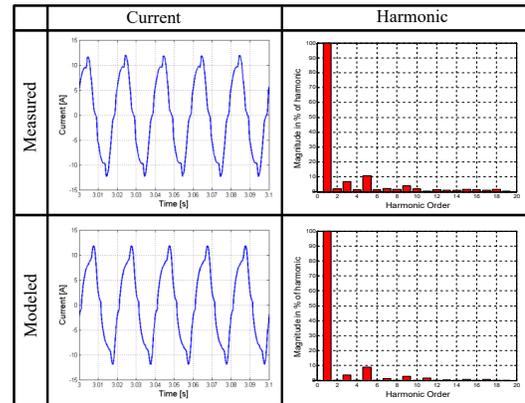


Fig. 12: Measured and simulated for masking load.

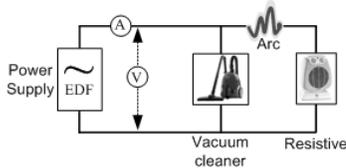


Fig. 11: Vacuum cleaner with an arc fault and drill configuration.

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