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Ning Dang, Nader Djelidi, Gustavo Adrián Echeveste Salazar, Alain Walcarius, Liang Liu, et al.. Integrated probe for electrochemical analysis of small volume droplets. *Sensors and Actuators B: Chemical*, 2021, 347, pp.130542. 10.1016/j.snb.2021.130542 . hal-03355536

HAL Id: hal-03355536

<https://hal.univ-lorraine.fr/hal-03355536>

Submitted on 27 Sep 2021

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Integrated probe for electrochemical analysis of small volume droplets

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Abstract

Analysis of small volume droplets is increasingly important in biology, environment, and material science. In this work, an integrated probe consisting of a Pt microelectrode wrapped with an Ag/AgCl wire and inserted into an outer capillary filled with KCl is developed as sensor for electrochemical analysis of small volume droplets (20 μ L). With a 3D-printed holder, the design allows easy fabrication, dismantling and re-assembly, which is important for renewing the probe. The integrated probe shows acceptable ohmic drop with electrochemical impedance spectroscopy, thus offers reliable and reproducible potentiometric and voltammetric measurements in bulk solutions. The ring-shaped opening between the inner microelectrode and the outer capillary also enables homogenous current distribution when applying potential between Pt and Ag/AgCl. Based on this, two droplet systems mimicking atmospheric corrosion are *in-situ* studied: (1) Fe^{3+} droplet on bare and silane-coated steel; (2) Cu^{2+} in a H_2SO_4 droplet

on copper. The concentration of $\text{Fe}^{3+}/\text{Fe}^{2+}$ and Cu^{2+} in the droplet is monitored with time, allowing interfacial corrosion reactions between the droplet and the substrate to be studied.

Keywords: Microelectrode; Droplet analysis; Potentiometry; Anodic stripping voltammetry; Atmospheric corrosion.

1. Introduction

Droplets of small volume are very common in nature, such as saliva on the tongue [1–4], sweat on the skin[5–7], as well as rain drops on solid supports like leaves[8] or metals [9–11]. Besides, artificial occasions, such as highly humid chamber [12,13] and ink-jet printing [14], may also generate small droplets on sample surfaces. Thus, the chemical analysis of small droplets is highly desired. One strategy is to transfer the sample for spectrometric or electrochemical analysis, typically through microfluidic devices [15–18] and screen-printed electrodes [19–22]. These sensors can be highly sensitive and are well developed and commercialized. However, they consume the sample and therefore can only provide static chemical information of the droplet. For tracking the evolution of chemistry in the droplet, miniaturized sensors that can *in-situ* analyse small volume samples are required. This may allow studying the interfacial chemistry between the droplet and the support surfaces.

As a direct bridge between chemistry and instrument measurable electrical signals, electrochemical analysis is naturally ideal for constructing *in-situ* miniaturized sensors. This is usually achieved by microelectrodes due to the high spatial and temporal resolution [23–26]. The fabrication of microelectrodes is matured and widely applied for scanning electrochemical microscopy. Nevertheless, for electroanalysis in a small droplet, it is essential to have at least

another reference electrode. The technical challenge is to combine the microelectrode with the micro-reference electrode and have both in contact with the same droplet. A promising approach is to use theta-capillary. Souto et al. developed dual microelectrode probes that consist of a Mg^{2+} ion-selective electrode and a reference electrode for monitoring the concentration evolution of Mg^{2+} in the close vicinity of Mg substrate [27]. Unwin *et al.* developed scanning electrochemical cell microscopy for carrying out local electrochemical measurements revolutionarily in a nanometer-sized meniscus that spreads on a sample surface [28,29]. Due to the presence of two electrodes (one serves as reference electrode) in the probe, it allows approaching the probe and detecting the droplet/sample contact even for insulating samples [30]. The system has been used for studying various interfacial reactions between samples and droplets, including electrocatalysis [31–42], charge-discharge in batteries [43–46], and corrosion [47–49], *etc.* However, these theta-capillary based working-reference dual electrodes face a technical challenge of regeneration. They cannot be polished like classical single microelectrodes as the polishing paste or the debris may block the opening of the reference capillary.

Herein, we develop a new integrated probe for *in-situ* quantitative electrochemical analysis of small volume droplets on solid surfaces regardless of the nature of droplet and support. It allows monitoring the interfacial reactions between the droplet and the support with relatively high spatial resolution. A Pt microelectrode is wrapped with Ag/AgCl wire on its shield and is inserted into an external capillary filled with KCl electrolyte. The special design allows easy fabrication, dismantling and re-assembly, so that the probe can be completely regenerated by polishing the working electrode and replacing the electrolyte in the outer capillary. Moreover, the reference

electrode has a ring-shaped opening around the working electrode, providing an acceptable resistance and homogeneous current distribution for potentiometric and amperometric measurements. The integrated probe is characterized and calibrated in bulk solutions of large volume, and then is approached to 20 μL droplets for electrochemical analysis. It is proved to be useful in *in-situ* and spatially-resolved corrosion analysis [50]. Besides, more possibilities in biological analysis and environmental monitoring should also be seen in the future by sensing small droplets.

2. Experimental

2.1. Chemical and materials

The metal wires (Pt of 25 μm and 1 mm diameter, Ag of 50 μm diameter) and the Pt foil are purchased from ChemPUR, Germany. The inner glass capillary for sealing Pt microelectrode is purchased from Sutter Instrument (BF150-75-10, inner diameter = 0.75 mm, outer diameter = 1.5 mm). The outer glass capillary is customized by Hilgenberg GMBH with inner diameter = 1.8 mm, outer diameter = 2.4 mm. Metal plates of Fe (99.99%, ChemPUR) and Cu (99.9%), as well as microscope glass slides, are used as samples for droplet analysis. The metal plates are polished with SiC paper up to 4000 grit and then cleaned by sonication in ethanol and acetone. For comparison, one Fe plate is coated with silane by electrodeposition. The deposition solution consists of 3.3 vol. % methyltriethoxysilane (98 %, Sigma), 1.15 vol. % tetraethoxysilane (98 %, Sigma), 2/1 (v/v) ethanol/water mixed solvent and 0.2 M NaNO_3 , with pH adjusted to 4 using HCl. The solution is pre-hydrolyzed at 35 $^{\circ}\text{C}$ for 48 h. The electrodeposition is carried out on Fe plate at -1.4 V (vs. Ag/AgCl) for 300 s, and the film is rinsed by water and dried before use.

[51–53]. All the chemicals used in this work are reagent grade and used without further purification.

2.2. Preparation of the integrated probe

The integrated probe consists of three parts: a Pt micro-disk electrode, an Ag/AgCl wire, and an outer capillary filled with electrolyte, as illustrated in **Fig. 1A**. The Pt micro-disk electrode is prepared with the same way as for scanning electrochemical microscopy measurements. A 25 μm diameter Pt wire is sealed into a pulled glass capillary by epoxy resin. The outer diameter of the original capillary is 1.5 mm, and after pulling it has an outer diameter of *ca.* 50 μm at the tip, which is about two times as that of the Pt wire. The Ag/AgCl wire is prepared by oxidizing a 50 μm diameter Ag wire in 0.1 M KCl solution at 0.12 V (*vs.* Ag/AgCl) for 30 s. After rinsing with deionized water, the wire is wrapped around the glass shield of Pt microelectrode and fixed with tacky glue. The outer capillary with 1.8 mm inner diameter is pulled to have a short tip of *ca.* 1 cm. It is then polished to have desired inner diameter of opening. The Pt micro-disk electrode stick with Ag/AgCl wire is inserted into the outer capillary and fixed together with screw in a 3D printed holder that allows fixing to a motor for positioning the probe. The last step is to soak electrolyte into the integrated probe through the thin gap at the tip between the inner electrode and the outer capillary to obtain a real reference electrode. For easily dismantling the outer capillary and refreshing the surface of inner microelectrode, 0.1 M KCl aqueous solution is filled as electrolyte rather than agar gel that is sometimes used [54]. The photographs of fabrication of the integrated probe are shown in **Fig. 1B**. We recommend using Cu wire with insulating coating to make the electrical contact for both the Pt microelectrode

and the Ag/AgCl wire to avoid short contact between them.

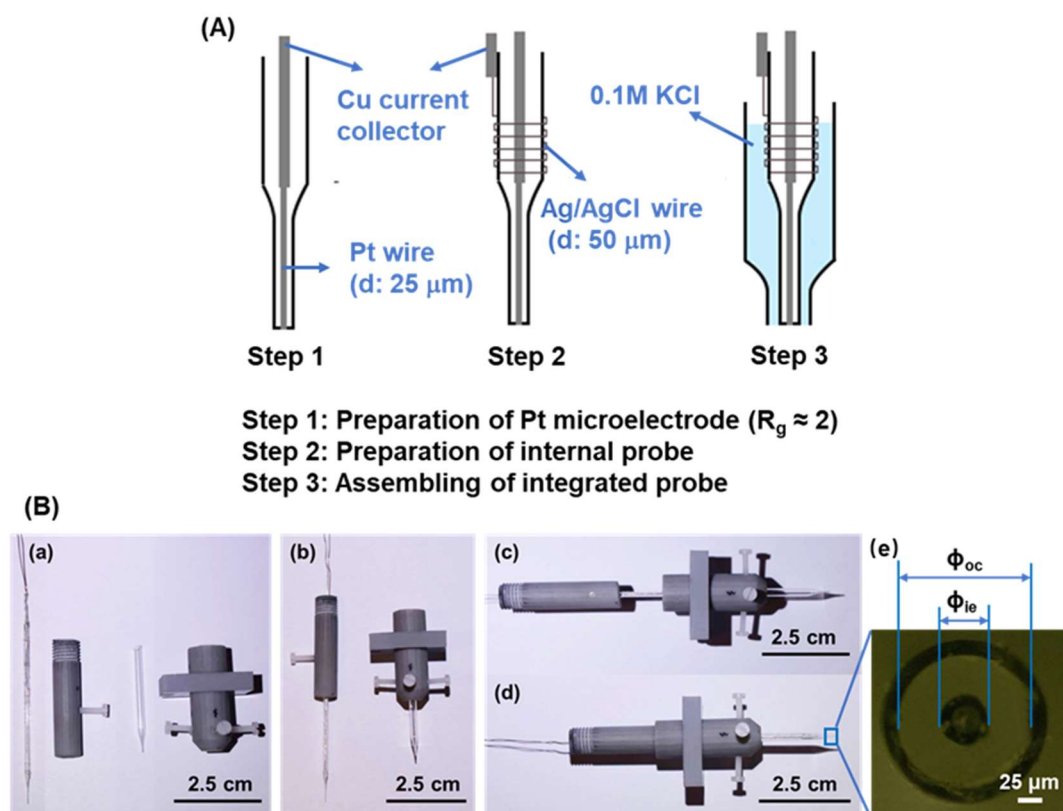


Fig. 1. (A) Scheme of the fabrication of integrated probe. (B) (a-d) Photographs illustrating different steps of the fabrication, (e) tip of the integrated probe, gap width (W) = inner

diameter of outer capillary (ϕ_{oc}) – outer diameter of inner electrode (ϕ_{ie}).

A major technical advantage of this design is the ease of fabrication and refreshing of the probe. All the three parts, namely the Pt micro-disk electrode, the Ag/AgCl reference electrode and the outer glass capillary, do not have strict dimension requirement. They can be easily dismantled and remounted. After dismantling the probe by removing the outer capillary, the inner microelectrode can be polished on a home-made polisher [55], as shown in the *Video*. It is mounted on the polisher, with both the polishing plate and the electrode rotating. The microelectrode is approached to gently touch a 0.3 μm diamond lapping film attached on the polishing plate. During polishing, the probe surface is rinsed by water. Generally, a few seconds

is enough for refreshing the probe. Afterwards, the outer capillary is mounted again and the electrolyte is refilled. If necessary, the Ag/AgCl wire can also be regenerated by re-oxidation of Ag. This means that the integrated probe can be easily and completely refreshed, which is highly important for practical applications in electrochemical analysis. Moreover, the Ag/AgCl wire has much higher area than the Pt microelectrode, so it can also serve as counter electrode in a two-electrode system for amperometric measurements. The ring-shaped gap between the inner microelectrode and the outer capillary allows uniform symmetrical current distribution. Like classical reference electrodes, the integrated probe can be stored by immersion in the KCl solution when not in use.

2.3. Characterization of the integrated probe

The integrated probe is characterized by electrochemical impedance spectroscopy (EIS), potentiometry and cyclic voltammetry (CV) in bulk electrolyte solutions of large volume (*ca.* 20 mL). EIS is performed in 0.1 M KCl solution for measuring the resistance of the reference electrode of the integrated probe. The Ag/AgCl wire of the integrated probe is connected as working electrode (WE), a commercial Ag/AgCl electrode is used as reference electrode (RE) and a Pt foil is used as counter electrode (CE). The measurement is carried out at open circuit potential (OCP) with a 10 mV sinusoidal perturbation in the frequency range of 100 kHz to 0.1 Hz on an Autolab potentiostat (PGSTAT 302N, Metrohm).

The potentiometry of the integrated probe is carried out in $\text{Fe}^{3+}/\text{Fe}^{2+}$ and $[\text{Fe}(\text{CN})_6]^{3-}/[\text{Fe}(\text{CN})_6]^{4-}$ redox couple solutions. The $\text{Fe}^{3+}/\text{Fe}^{2+}$ solutions are prepared by dissolving $\text{Fe}_2(\text{SO}_4)_3$ and FeSO_4 in 0.1M KCl electrolyte with the ratio of 50:1, 10:1, 1:1, 1:10, 1:50 (in mM). In order to inhibit

the hydrolysis of the $\text{Fe}^{3+}/\text{Fe}^{2+}$, pH of the solutions was adjusted to *ca.* 1.5 with H_2SO_4 . The $[\text{Fe}(\text{CN})_6]^{3-}/[\text{Fe}(\text{CN})_6]^{4-}$ solutions are prepared by dissolving $\text{K}_3\text{Fe}(\text{CN})_6$ and $\text{K}_4\text{Fe}(\text{CN})_6$ in 0.1M KCl electrolyte with the ratio of 1:0.1, 0.164:0.1, 0.1:0.1, 0.1:0.164, 0.1:1 (in mM). The OCP between the Pt microelectrode and the Ag/AgCl reference electrode of the integrated probe is recorded by a voltammeter with high input resistance (Keithley 6430). In order to examine the response time of the integrated probe, the OCP was also record in $\text{Fe}^{3+}/\text{Fe}^{2+}$ solutions while changing the concentration ratio by adding drops of Fe^{3+} or Fe^{2+} every 600 s. The solution was kept under stirring for rapid and homogeneous mixture of the species.

The CV of the integrated probe is measured in a solution with 1 mM ferrocenedimethanol (FcMeOH) and 0.1 M KCl. The Pt microelectrode of the integrated probe is connected as WE. For two-electrode system that involves only the integrated probe, the Ag/AgCl wire is connected as both RE and CE. A three-electrode system that connects the Ag/AgCl wire of the integrated probe as RE and a separate Pt wire (1 mm diameter) as CE is also measured for comparison. The potential is scanned in the range of 0 to 0.6 V at 10 mV/s scan rate.

2.4. Electrochemical analysis in droplets

Fig. 2 illustrates the setup of droplet analysis using the integrated probe. A major concern is to keep the humidity of the environment to minimize the evaporation of the droplet. The sample is placed in a 3D printed plastic chamber with water reservoir. The hole at the top of the chamber allows putting the droplet by micropipette and inserting the integrated probe. Afterwards, the gap between the probe and the chamber is rapidly sealed with parafilm, and then the probe is approached to be in contact with the droplet.

20 μL droplets of $\text{Fe}(\text{NO}_3)_3$ in concentration of 1, 5, 10, 25, 50 mM are dropped on bare and silane-treated Fe plates for potentiometric measurements. The measurement configuration is the same as potentiometric characterization of the probe in bulk solution. For amperometric measurements, 20 μL droplets of 0.1 M H_2SO_4 are dropped on Cu plates, and concentration of Cu^{2+} is traced by anodic stripping using the integrated probe. The Pt microelectrode is connected as WE, and the Ag/AgCl wire is connected as RE and CE for a two-electrode system. The stripping is carried out by preconcentration of Cu at -0.2 V for 30 s followed by CV scans from -0.08 to 0.6 V at scan rate of 50 mV/s. The calibration of Cu stripping was achieved by the integrated probe in 0.1 M H_2SO_4 and CuSO_4 solutions with Cu^{2+} concentration of 1, 2.5, 5, 10, 50 mM. For both potentiometric and amperometric measurements, control experiments are carried out on glass slides with the same protocols.

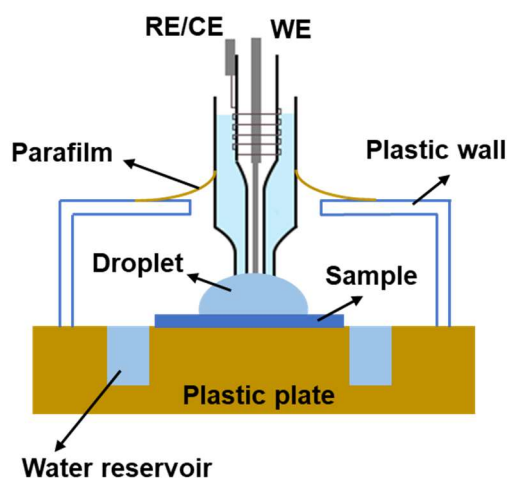


Fig. 2. Scheme of the setup for electrochemical droplet analysis using integrated probe.

3. Results and Discussion

In the integrated probe, the inner Pt microelectrode serves as WE, and the Ag/AgCl wire with KCl electrolyte serves as RE. Therefore, it is essential to evaluate the stability and reliability of

the configuration especially for the Ag/AgCl RE. This is first carried out in bulk solutions by measuring their electrochemical behavior. Three aspects are tested: the ohmic resistance in the gap between the inner microelectrode and the outer capillary, the potentiometric and voltammetric measurements in standard redox solutions. As a further step, the probes are used for droplet analysis. Potentiometric analysis is carried out by following the open circuit potential of a Fe^{3+} droplet on Fe plate, and amperometric analysis of Cu^{2+} by anodic stripping is measured in a H_2SO_4 droplet on Cu plate. The results allow analyzing the evolution of metal ion concentration, which reflect the corrosion reactions between the droplet and the metals.

3.1 Evaluation of the integrated probe in bulk solutions

A major criterion for RE is the ohmic resistance that originates from the ion exchange between its internal electrolyte and the external measurement media, as it determines the ohmic drop in electrochemical measurements [56]. In the integrated probe, it is mainly affected by the gap between the inner microelectrode and the outer capillary, which should allow ion exchange yet have low rate of leakage. Here, the ohmic resistance is measured by EIS in a three-electrode system, with the Ag/AgCl wire of the integrated probe as WE, a commercial Ag/AgCl reference electrode as RE and a Pt foil as CE as illustrated in **Fig. 3A** [57,58]. In this case, the DC resistance at high frequency mainly reflects the ion transfer resistance of the gap. From the Nyquist diagram (**Fig. 3B**), it is seen that the interceptions of the curves with the real axis tested with outer capillaries (*ca.* $\geq 46 \text{ k}\Omega$) are orders of magnitude higher than that measured without the outer capillary (*ca.* $40 \text{ }\Omega$). In addition, the DC resistance increases with decreasing the gap width W between inner electrodes and outer capillaries. This confirms that the DC resistance

mainly reflects the ion exchange through the gap. The dramatic increase in the DC resistance to hundreds of k Ω might also introduce artifacts for high frequency measurements, which could be the reason for the striking distortion of the spectra.

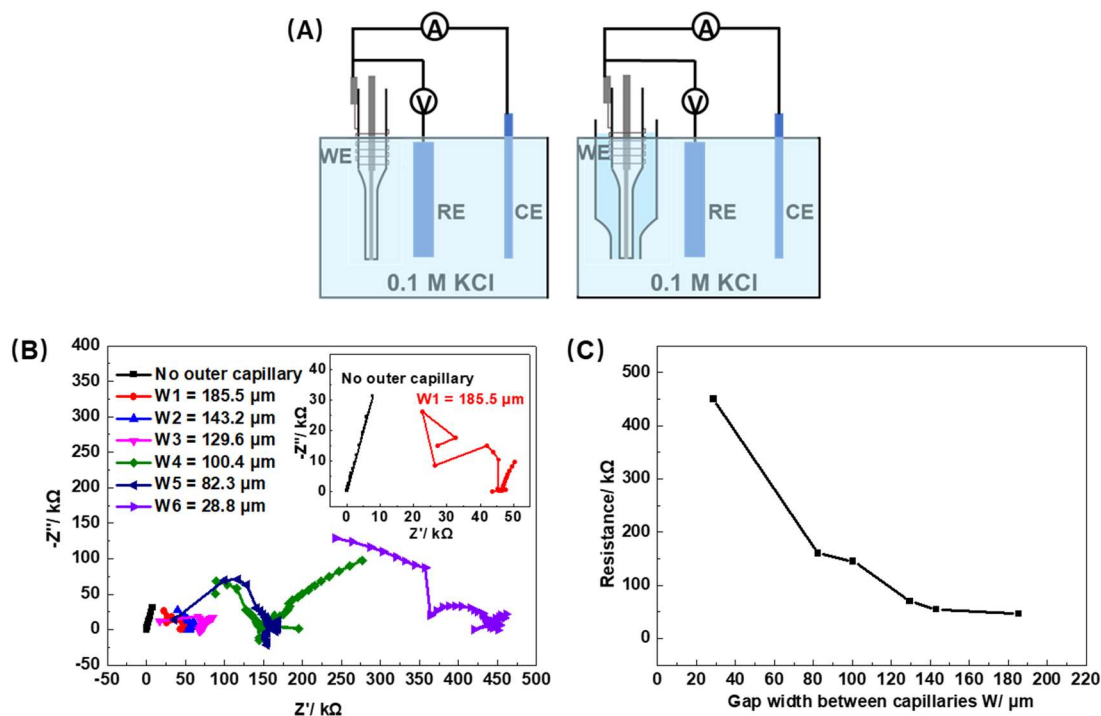


Fig. 3. (A) Scheme of EIS measurement; (B) Nyquist plots of Ag/AgCl wire of the integrated probe in 0.1 M KCl solution with different gap width (W) between inner electrodes and outer capillaries; (C) Ion transfer resistance of integrated probes with different gap width.

Considering that the WE has a diameter of 25 μm , the double layer capacitance is about 98 pF (in 0.1 M KCl solution [59]), and the current in typical CV or amperometric measurements usually does not exceed 10 nA. Based on the measured resistance value, one may estimate that the ohmic drop of the system is in the range of 1 - 4 mV, and the time constant is around 40 μs . This is acceptable for most of the electrochemical measurements. Besides, when the gap width is in the range of *ca.* 129 to 185 μm , the DC resistance has very similar values (**Fig. 3C**), indicating that the cell properties are not sensitive to the gap width in this range. This leaves

flexibility for polishing the outer capillaries, and EIS measurement may serve as a tool for quality control of the integrated probe. Generally, we recommend to have a gap width around 130 μm , as smaller gap would yield a significant increase in the DC resistance, while larger gap might increase the risk of solution leakage.

The potentiometric analysis of the integrated probe is carried out in redox couple solutions by measuring the open circuit potential between the inner Pt microelectrode and the Ag/AgCl wire in the outer capillary, as illustrated in **Fig. 4A**. The probe is initially placed in air, and then it is approached to immerse in the redox solution when the potential is monitored. **Fig. 4B** shows the potential of the probe measured in $\text{Fe}^{3+}/\text{Fe}^{2+}$ redox couple solutions with different ratio. The small plateau in the first 20 s corresponds to the “free” potential of the probe in air, which is meaningless. When the probe is in contact with the solution, the potential changes quickly before reaching equilibrium. The response time of the probe when initially approaching from air to solution is *ca.* 50-150 s depending on the solution. However, the response is faster for the variation of concentration when the probe is already immersed in the solution, as shown in **Fig. 4D**. The response time is reduced to *ca.* 30 s, which is much longer than the RC time constant of WE. This might be attributed to the slow ion exchange in the narrow gap between inner and outer capillaries. Similar phenomenon can also be seen in ion-selective electrodes where membranes with limited ionic conductivity are used. However, once the equilibrium is reached, the potential is highly stable for a long time of measurement. The potential versus the $\text{Fe}^{3+}/\text{Fe}^{2+}$ ratio can be well fitted to Nernst equation as shown in **Fig. 4C**. The slope is *ca.* 59 mV, and the R^2 is 0.996. The potential also accurately reflects the dynamic change of redox ratio in **Fig. 4D**. Similar trends are also seen with $\text{Fe}(\text{CN})_6^{3-}/\text{Fe}(\text{CN})_6^{4-}$ redox probes (**Fig. S1**), and the results

confirm that the integrated probe is reliable for potentiometric analysis in redox solutions.

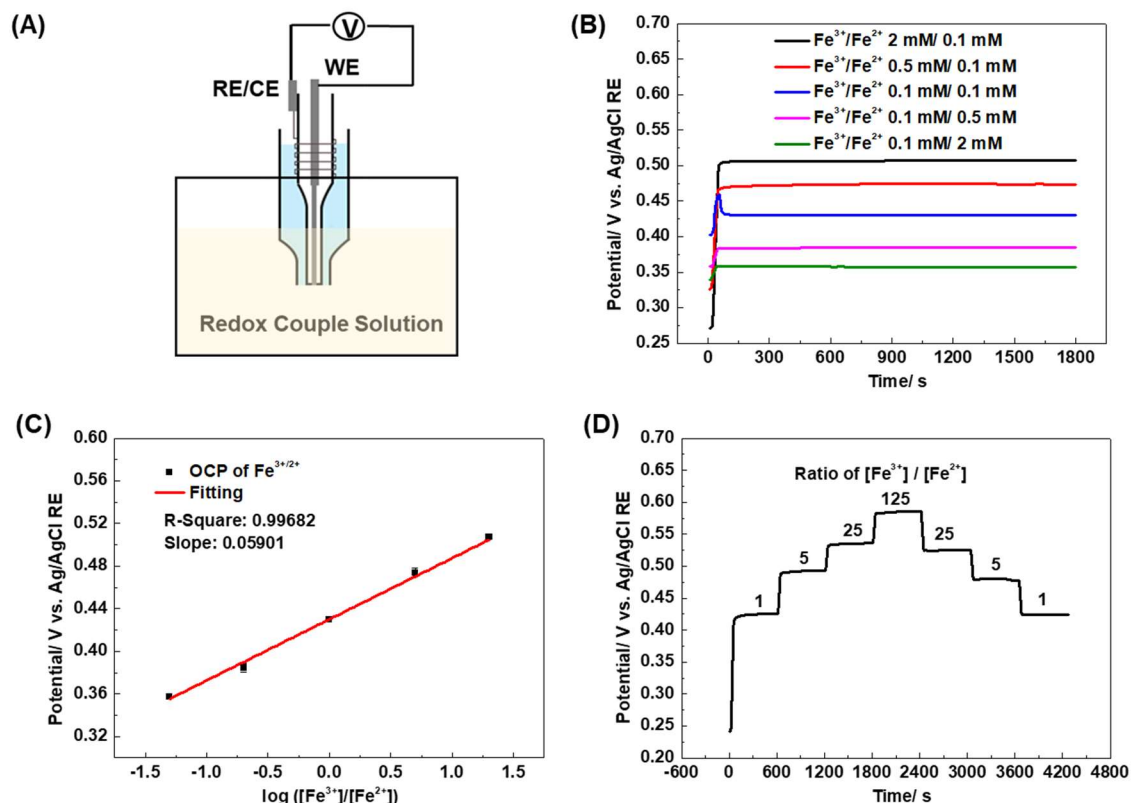


Fig. 4. (A) Scheme of potentiometric measurements of the integrated probe in bulk solutions; (B) Potential variation in $\text{Fe}^{3+}/\text{Fe}^{2+}$ redox solutions with different concentration ratio; (C) Potential versus $\log([\text{Fe}^{3+}]/[\text{Fe}^{2+}])$; (D) Potential steps following the variation of $[\text{Fe}^{3+}]/[\text{Fe}^{2+}]$ ratio in the solution.

Besides potentiometry, the integrated probe is also used for voltammetric measurements. Different configurations are compared for the measurement and illustrated in **Fig. 5A**: (a) Pt microelectrode as WE, Ag/AgCl wire as quasi-reference electrode (QRE) without outer capillary, and a Pt wire of 1 mm diameter as CE; (b) Pt microelectrode as WE, Ag/AgCl wire with 0.1 M KCl in the outer capillary as RE, and a Pt wire of 1 mm diameter as CE; (c) Pt microelectrode as WE, and Ag/AgCl wire in 0.1 M KCl in the outer capillary connected as both

RE and CE. The results show classical sigmoidal shape voltammogram of microelectrodes in 1 mM FcMeOH solution, and there is no significant difference between the three configurations (Fig. 5B). Moreover, the measurements are highly reproducible for multiple experiments with configuration (c) as shown in *Supplementary Information* (Fig. S2). This suggests that the Ag/AgCl wire in 0.1 M KCl in the outer capillary functions well as RE, and it can even be used as CE as the area of Ag/AgCl is much higher than that of Pt microelectrode so that the polarization is negligible. The resistance of the gap between Pt microelectrode and the outer capillary appears to have no significant influence on the results, which is due to the low current in the measurement. This suggests that the integrated probe can also be used for voltammetric analysis in a two-electrode system, with the Pt microelectrode as WE and the Ag/AgCl wire in 0.1 M KCl in the outer capillary as RE and CE.

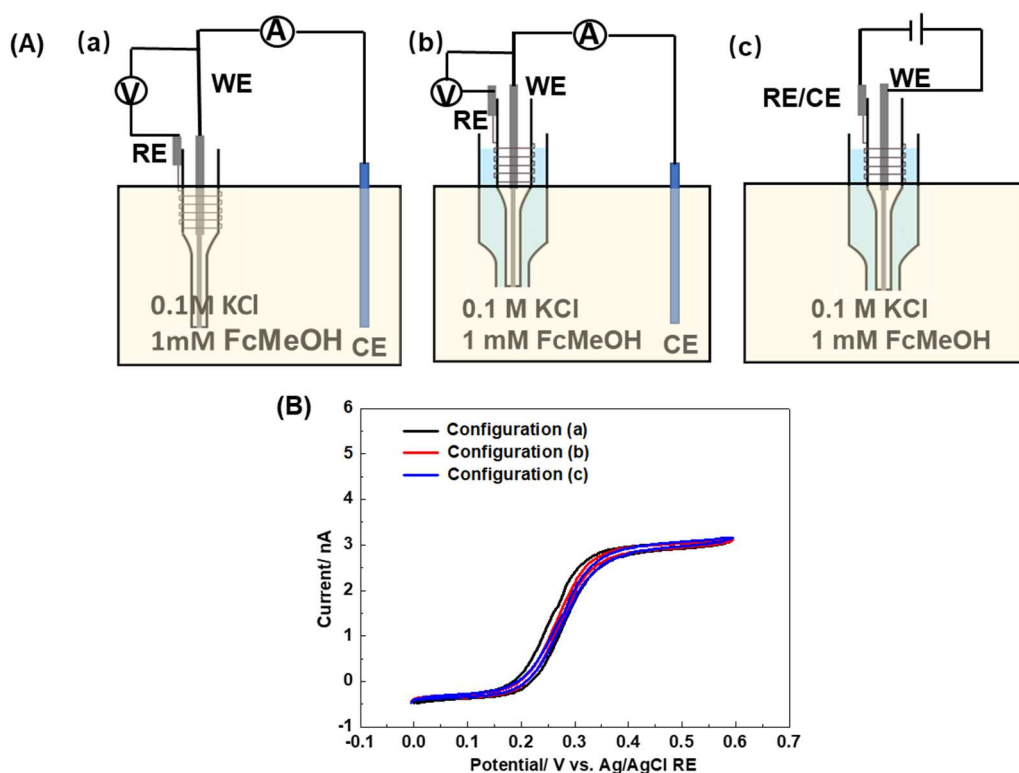


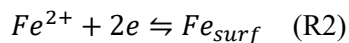
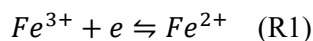
Fig. 5. (A) Schemes of CV in 1mM FcMeOH solution by integrated probe; (B) CV of the

integrated probe in 1mM FcMeOH solution with different configurations. Scan rate in CV measurement is 10 mV/s.

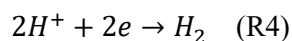
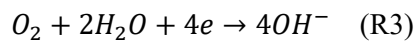
The results above show that the integrated probe has acceptable ohmic resistance for the gap between the Pt microelectrode and the outer capillary. This allows the probe to be reliably used for potentiometric and voltammetric measurements in bulk solutions with large volume.

3.2 Potentiometric measurements of Fe^{3+} droplets on Fe plate

As designed, the small size of the tip of the integrated probe allows electrochemical measurements in small droplets. This is especially useful for tracking the evolution of chemistry of droplets, which may further indirectly reveal the kinetics of reactions at the droplet/substrate interface. For example, Turyan *et al.* analyzed the oxidation kinetics of therapeutic proteins in 150 μ L droplets by potentiometry for rapid screening of their activities [60]. A classical qualitative method for evaluating the corrosion activity of metals is by droplets that change color upon reaction with the metal, *e.g.* $CuSO_4$. Here, we demonstrate an example of potentiometric analysis using the integrated probe for tracking the reduction of Fe^{3+} in a 20 μ L droplet by steel substrate. The main reactions are as follows:



Besides, in aerated droplets, the reduction of O_2 and H^+ may also drive the corrosion of Fe:



Considering the limited concentration of dissolved O₂ and the acidity of solution, R1 and R2 are expected to be dominant in the system. Thus, the concentration ratio between Fe³⁺ and Fe²⁺ in the droplet follows Nernst Equation, which can be measured by the potential of the integrated probe:

$$E_{probe} = E_{Fe^{3+}/Fe^{2+}}^{0'} - \frac{RT}{F} \ln \frac{[Fe^{2+}]}{[Fe^{3+}]} \quad (Eq. 1)$$

where $E_{Fe^{3+}/Fe^{2+}}^{0'}$ refers to the formal potential of Fe³⁺/Fe²⁺ redox couple, R is the ideal gas constant (8.314 J·K⁻¹·mol⁻¹), T is the temperature (298 K) and F is the Faradic constant (96,485 C·mol⁻¹). By measuring the potential of the probe in 1:1 Fe³⁺/Fe²⁺ solution, the potential of the reference electrode could be calibrated by Eq. 1 taking into consideration the activity coefficient of Fe²⁺ and Fe³⁺. As the electrode is home-made, the unoptimized oxidation of Ag wire (especially considering its small diameter) and the solution exchange between the electrode and the sample may cause non-negligible deviation of its potential. Thus, it is recommended to calibrate the reference electrode potential before use.

Knowing the initial concentration of Fe³⁺ and Fe²⁺ in the droplet, with the stoichiometry and the measured potential of the probe, one may derive the concentration of Fe³⁺ and Fe²⁺ at any time in the droplet. They can be expressed as follows:

$$[Fe^{3+}] = \frac{\frac{3}{2}[Fe^{3+}]_0 + [Fe^{2+}]_0}{\frac{3}{2} + \exp\left[\frac{F}{RT}(E_{Fe^{3+}/Fe^{2+}}^{0'} - E_{probe})\right]} \quad (Eq. 2)$$

$$[Fe^{2+}] = \frac{\frac{3}{2}[Fe^{3+}]_0 + [Fe^{2+}]_0}{1 + \frac{3}{2}\exp\left[\frac{F}{RT}(E_{Fe^{3+}/Fe^{2+}}^{0'} - E_{probe})\right]} \quad (Eq. 3)$$

where $[Fe^{3+}]_0$ and $[Fe^{2+}]_0$ refer to the initial concentration of Fe³⁺ and Fe²⁺ in the droplet, respectively. As a result, the concentration variation as a function of time can be tracked, and it reflects the kinetics of the two reactions R1 and R2, notably the latter which corresponds to the oxidation reactivity of the steel surface.

Fig. 6 shows the variation of the probe potential as a function of time for 20 μL droplets on bare steel, silane-coated steel and glass substrates. In all measurements, the potential takes *ca.* 100 s to stabilize. Afterwards, the potential is almost constant in the droplet on glass substrate, and

the value is the same as that measured in bulk solution. This suggests that after the response time of the integrated probe, the potentiometric measurements are reliable in small droplets. When the droplet is on bare steel substrate, it is seen that the potential decreases sharply until *ca.* 400s before reaching a plateau. This can be explained by the oxidization of Fe plate, which consumes Fe^{3+} in the droplet and generates Fe^{2+} following the redox reactions R1 and R2. For comparison, we also tested the potentiometry of Fe^{3+} droplet on silane treated Fe plate. The silane treatment is a known method for temporary protection of metals against corrosion [51–53]. The general trend of the results is the same as on bare Fe plate, but the initial potential decrease is less steep, and the final equilibrium potential is more positive. This suggests that the generation of Fe^{2+} is slower, on silane-treated Fe plate than on bare Fe plate, which qualitatively supports the expected corrosion inhibition effect. Nevertheless, this inhibition is less significant (**Fig. 6B**) with the increase of Fe^{3+} concentration. This might be related to the stronger attack of the silane film in more harsh media with higher concentration of the oxidant. Similar trends are also seen with other concentration of Fe^{3+} (**Fig. S3**). Similar experimental systems have also been used in scanning electrochemical microscopy for analyzing localized corrosion of Fe, where Fe substrate is locally oxidized to Fe^{2+} and then Fe^{2+} is further oxidized to Fe^{3+} on the microelectrode contributing to the measured current [61].

Potentiometry has an advantage of not perturbing the electrochemical system. Thus, it is especially suitable for *in-situ* monitoring the variation of concentration of redox species with time, and only very small volume of analyte is required with miniaturized integrated probes. In theory, the results in **Fig. 6** make it possible to further quantitatively analyse the kinetics of both reactions R1 and R2. However, in practice, attention must be paid for the experimental control.

Rigorously, the potential measured from the integrated probe reflects only the surface concentration of Fe^{3+} and Fe^{2+} near the probe. Thus, the derivation of *Eqs. 2 and 3* from *Eq. 1* requires an approximation that the concentration distribution is always uniform in the droplet. When the droplet is static on the surface, this approximation is unlikely fulfilled considering the size of the droplet. Assume the droplet has a contact angle of 60° with a flat surface, a 20 μL droplet has a height of *ca.* 0.156 cm. This will take *ca.* 76 s for an analyte generated on the sample surface to reach the top of the droplet (approximately taking linear diffusion with diffusion coefficient $2 \times 10^{-5} \text{ cm}^2/\text{s}$) where the integrated probe is likely positioned. Another concern is the shape of the droplet, which depends on the contact angle and changes due to the capillary force when in contact with the integrated probe. This complicates the geometry for simulating the electrochemistry with mass transport in the droplet, even with the contact angle measured. Moreover, the response time of the probe is also an issue. From **Fig. 4D** and **Fig. 6**, it is clearly seen that the potential takes time to reach equilibrium. This limits the time resolution of the measurement, especially when the potential rapidly changes with time such as between 100 and 300 s in **Fig. 6**. Besides, other redox reactions such as R3 and R4 may also interfere the analysis, leading to mixed potential where kinetic effect shall be considered. These reactions may even become dominant when the Fe^{3+} in the droplet is nearly fully consumed by Fe surface. With all these considerations, the experiments need to be very carefully designed for meaningful quantitative analysis of the kinetics of the interfacial reactions between the droplet and the sample.

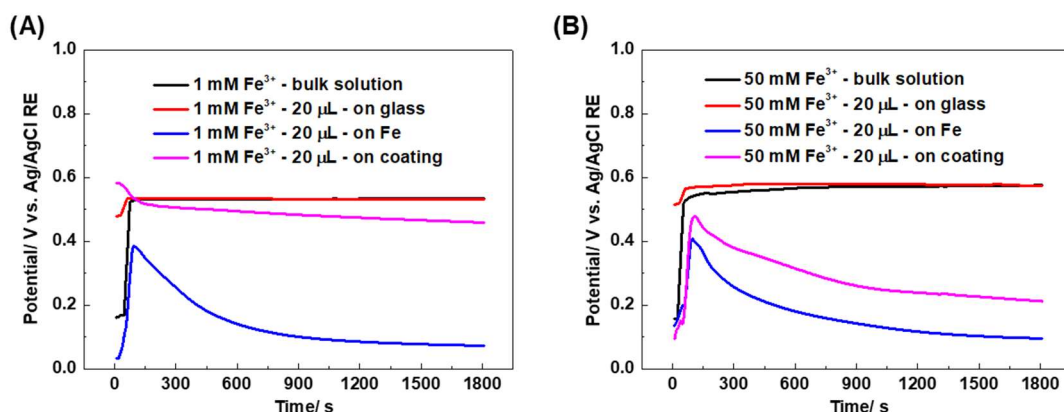


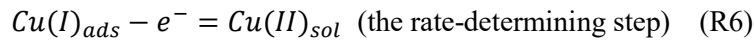
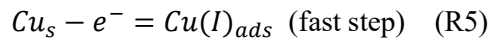
Fig. 6. OCP measurements by integrated probe in Fe³⁺ bulk solution, 20 µL Fe³⁺ droplet on insulating glass, bare and silane-treated Fe substrates. (A): 1 mM Fe³⁺, (B): 50 mM Fe³⁺.

3.3 Anodic stripping voltammetry in H₂SO₄ droplet on Cu plate

As shown in **Fig. 5**, the integrated probe can also be used for voltametric analysis by connecting the Ag/AgCl as both RE and CE. This is further extended to droplet analysis in the form of stripping voltammetry. Stripping voltammetry is a powerful electrochemical measurement for analyzing low concentration of species. With a preconcentration step, the detection limit can reach nM range [62,63], and it is ideal for electroanalysis of metal ions *via* electrodeposition followed by anodic stripping [64–67]. The electrode is naturally renewed after stripping, thus it can be used to monitor the change of metal ion concentration in a droplet during the corrosion process [68].

Here, we demonstrate a model system that mimics atmospheric corrosion of Cu in acidic spray. 20 µL of 0.1 M H₂SO₄ is dropped on Cu substrate, and the dissolution of Cu is followed by anodic stripping analysis of Cu²⁺ concentration in the droplet using the integrated probe. **Fig. 7A** shows the anodic stripping signals at different time measured *in-situ* in the H₂SO₄ droplet from the integrated probe. For each measurement, the integrated probe is pre-conditioned at –

0.2 V (Pt WE vs. Ag/AgCl RE/CE) for 30 s for pre-concentration in droplets, and then CV was performed from –0.08 to 0.6 V (Pt WE vs. Ag/AgCl RE/CE) for stripping Cu without moving the probe. It is seen that the area of the stripping peak increases as a function of time, which indicates the corrosion of Cu in the H₂SO₄ droplet. As the charge of Cu stripping is linear with the concentration of Cu²⁺ (calibration curve in **Fig. 7B**), one may derive the variation of Cu²⁺ concentration in the droplet, as shown in **Fig. 7C**. It is clearly seen that the signal is low in the first 25 minutes, and afterwards it increases with time. Considering that it takes less than 5 minutes for Cu²⁺ ions to diffuse from the substrate to the top of the droplet (same estimation as in section 3.4), this phenomenon cannot be only attributed to the lag of detection. According to Mattsson and Bockris [69] and other research workers [70,71], the anodic dissolution of copper takes place through two consecutive steps:



R5 refers to an incubation period, where the corrosion yields adsorbed Cu(I) species that do not dissolve in the solution [72]. This may explain the low concentration of Cu²⁺ analyzed from the droplet at the initial stage of corrosion. Later, the Cu(I) species are further oxidized (R6), then Cu²⁺ concentration increases rapidly, and can be followed by anodic stripping voltammetry.

The chemical analysis of the corrosion product in corrosive media is often used for evaluating the corrosion rate, which is a key characteristic for metallic structures. As compared with classical chemical analysis such as ion chromatography [73,74] and inductively coupled plasma atomic emission spectroscopy [75], the integrated probe does not consume the sample and requires only very small volume so that it has merits in *in-situ* measurements as demonstrated

in **Fig. 2**. The corrosion rate is often expressed as weight loss of the metal per time. In the case of H_2SO_4 droplet on Cu, the weight loss of Cu turns into Cu^{2+} ions in the droplet, thus it can be derived from the following equation:

$$\text{Corrosion rate} = \frac{V_{\text{droplet}}}{\rho_{\text{Cu}} A} \cdot \frac{d[\text{Cu}^{2+}]}{dt} \quad (\text{Eq. 4})$$

where ρ_{Cu} is the density of Cu metal, A is the wetted area of the droplet, V_{droplet} is the volume of the droplet. The corrosion rate is in the unit of thickness per time ($\mu\text{m}/\text{min}$), which can be calculated from the time derivative of **Fig. 7C**. This simple calculation does not take into account the formation of Cu(I) , but it could still qualitatively reflect the corrosion behavior. The results are shown in **Fig. 7D**. Note that two different areas (point 1 and point 2 in **Fig. 7C** and **Fig. 7D**) of the substrate are tested. The trend of corrosion is similar, but the exact rate is different. This is probably due to the inhomogeneity of the surface, which may sensitively affect the initial stage of corrosion. In another word, it suggests that the integrated probe may offer the possibility to evaluate the local corrosion rate in atmospheric corrosion.

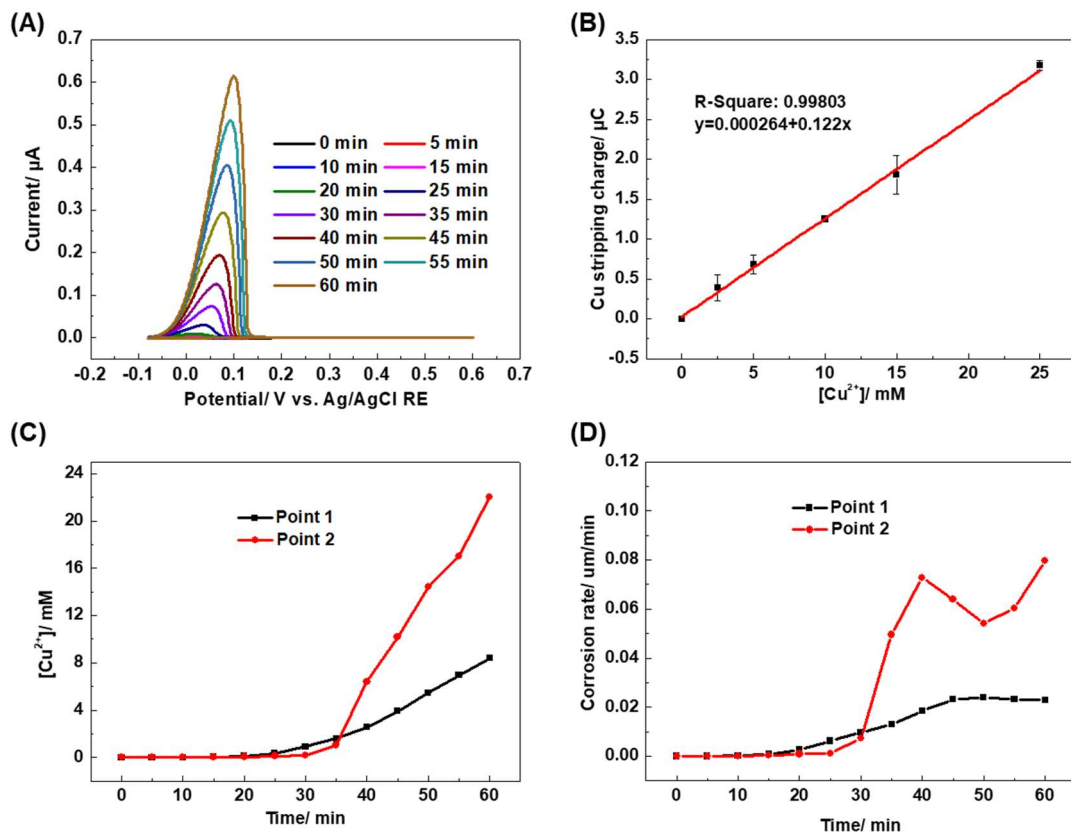


Fig. 7. (A) Anodic stripping signals of Cu measured in $20\ \mu\text{L}$ $0.1\ \text{M}$ H_2SO_4 droplet on Cu plate at different time with interval of 5 min; (B) Calibration curve of Cu stripping charge vs. concentration by the integrated probe in Cu^{2+} bulk solutions; (C) $[\text{Cu}^{2+}]$ in the droplet as the function of time; (D) The corrosion rate of Cu in $\mu\text{m/min}$, calculated with $\rho_{\text{Cu}} = 8.89\ \text{g/cm}^3$ and $A \approx 0.28\ \text{cm}^2$.

4. Conclusion

In conclusion, an integrated probe is developed for electrochemical analysis in small volume droplets. The integrated probe consists of a Pt microelectrode, an Ag/AgCl wire fixed on the shield of the microelectrode, and an external capillary soaked with electrolyte. With the customized holder, the probe can be easily separated and reassembled, which allows facile and thorough regeneration. The ohmic drop of the gap between the inner microelectrode and the

outer capillary is acceptable for both potentiometric and voltammetric measurements. The probe is carefully tested and calibrated in bulk solutions, and then is used for *in-situ* electroanalysis of 20 μL droplets. Two systems are tested: (1) potentiometric analysis of Fe^{3+} droplet on bare and silane-coated Fe; (2) anodic stripping voltammetry of Cu^{2+} in a H_2SO_4 droplet on Cu. In both cases, the results are in good agreement with the corrosion behavior of the substrate, and the corrosion rate can be analyzed. With the improvement of the experimental control, it is also foreseeable to quantitatively derive the kinetics of redox reactions in the droplet or at the droplet/substrate interface. This would be highly helpful for biomedical applications in future, where the analyte is usually in small quantity and quantitative results are expected from *in-situ* measurements.

CRedit authorship contribution statement

Ning Dang: Investigation, formal analysis, writing-original draft

Nader Djelidi: Investigation

Gustavo Adrián Echeveste Salazar : Investigation

Alain Walcarius: Supervision

Liang Liu: Methodology, funding acquisition, software, writing-review&editing

Mathieu Etienne: Conceptualisation, methodology, resources

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Acknowledgement

We gratefully acknowledge financial support from CNRS MOMENTUM Project (2018-2020).

The work is also supported by the Chinese Scholarship Council.

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