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Reconstitution of fruit powders: a process - structure - function approach

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## Graphical Abstract



Schematic explanation of the relationship between water activity and fruit powders behavior during reconstitution.

## Abstract

Reconstitution of six fruit powders, compacted and non-compacted, were studied. It appears that powder reconstitution behavior under sheared conditions was significantly different with regards to the water activity $\left(a_{w}\right)$. At low $a_{w}$, the powders exhibit a glassy state with a stiff surface measured by Atomic Force Microscopy and porous/angular shapes were observed by

Scanning Electron Microscopy. In that case, increasing the shear rate accelerated the kinetics of reconstitution by improving water penetration through particle surface pores thus reducing the reconstitution time. Therefore, the reconstitution is shear rate dependent. At high $a_{w}$, the powders are under a rubbery state with a soft surface and a smooth shape. Under these environmental conditions (i.e. above powder's glass transition temperature), increasing the shear rate did not improve their reconstitution. Therefore, the reconstitution kinetics is not shear-dependent in the stirring rate studied (from 800 to 1500 rpm ). It is suggested that the viscous layer created on the particle surface blocks the entrance of water for these powders rich in sugar and presenting low glass transition temperatures.

## Key words

Fruit powder; reconstitution; shear rate; glass transition temperature; compaction; water activity

## 1 Introduction

Fresh fruits are usually dried as they contain about $90 \%$ water by weight and reducing the water activity in the product allows for food preservation (i.e. reducing microbial and enzymatic activities). Indeed, browning and loss of nutritional value are typical of fresh fruits even at ambient temperature and relative humidity. In the powder form, the stability and the functionality of the ingredients composing fruits are maintained (Fitzpatrick and Ahrné, 2005). However, fruit powders contain a high quantity of low molar mass sugars with low glass transition temperature $\left(\mathrm{T}_{\mathrm{g}}\right)$ (Fang and Bhandari, 2011). The direct consequence is that fruit powders are highly hygroscopic and sticky at high temperatures but also at ambient temperature if the water content is not well mastered. This feature causes the powder
adhesion to surfaces and powder caking during the storage, which affects the quality of the final product (Gabas et al., 2007; Fabra et al., 2011). The $\mathrm{T}_{\mathrm{g}}$ is one of the most important parameters to take into account during powder storage. Indeed, the phenomenon of glass transition is the gradual and reversible transition of amorphous materials from a hard and "glassy" state into a viscous and rubbery state as the temperature and/or the moisture content is increased. The glass transition is also linked to the water activity and water as a strong plasticizer decreases the $\mathrm{T}_{\mathrm{g}}$. Also, the glass transition temperature depends on the molecular mass as the $\mathrm{T}_{\mathrm{g}}$ of monosaccharides, disaccharides, oligosaccharides and polysaccharides increases with increasing their molecular mass (Roos, 2002). If the glass transition is reached during powder storage, unexpected phenomena can happen that affect powder functionality such as reconstitution ability. One way of influencing this powder functionality is the granulation process.

Granulation is a particle size-enlargement process carried out to improve flowability, compaction and homogeneity of powders. This is an important process in many industries including the food, pharmaceuticals and chemical industries. Roller compaction is a process used for dry granulation typically employed in the food industry to increase the flowability of a powder by forming granules of large size and density (Kleinebudde, 2004). During this processing step, a powder blend passes through two counter-rotating rolls that compact the blend into ribbons. The ribbons subsequently are milled into granules of a desired size distribution. This granulation process induces structural and physical changes by increasing the size of the particles and the voids between particles, but also by playing on powder bulk properties, especially by decreasing the bulk density (Rajniak et al., 2007). As a consequence, the wetting step is improved by the production of particles with large pores, which facilitate the entrance of water into particles (Hogekamp and Schubert, 2003). Dispersibility is also
related to the increased particle size (Goalard et al., 2006). Thus, granulation will impact the reconstitution ability.

Reconstitution of powdered ingredients is of particular importance to both manufacturers and consumers as a target of consumption quality (Fang et al., 2011). Reconstitution is highly dependent of both operating conditions and material properties. The objective is to restore the fresh product functional properties, especially for heat-sensitive food products such as vegetables and fruits powders (Lopez-Quiroga et al., 2019). Reconstitution of food powder generally consists of four steps or phases: wetting of powder particles, sinking, dispersing, and particles completely dissolving in solution (Forny et al., 2011; Mitchell et al., 2015). Wetting is the first step where the particles contact liquid, the physicochemical properties of particle surface is of major importance for improving initial step. Dispersing and dissolution are the critical phases where primary particles start to release materials from the particle surface into the liquid. Once any of these steps is limited, the time for the whole reconstitution is prolonged. Particularly, in the case of fruit powders, the dissolution cannot be fully achieved due to the presence of many insoluble polysaccharides. Additionally, different steps can overlap that makes understanding the global rehydration process more complicated (Schubert, 1993).

The influence of reconstitution conditions (stirrer speed, mixing systems, temperature, and viscosity) is also known to influence the reconstitution time. For dairy powders, authors (Jeantet et al., 2010; Andre et al., 2012) show that increasing temperature and/or agitation resulted systematically in decreasing the reconstitution time. Also, their respective influences were compared and increasing the temperature by $4{ }^{\circ} \mathrm{C}$ was found to have the same
influence on reconstitution time than multiplying by two the stirring speed. On the best knowledge of the authors, this type of study crossing the impact of the process parameters were never done on fruit powders. Because of various origins, particle size and shape distributions, chemical composition, surface composition, and physical properties, reconstitution is highly variable. Again, many data were acquired for dairy powders (Gaiani et al., 2006, 2007a, 2007b, 2009), hydrocolloids (Wangler and Kohlus, 2018), biopolymers (Wangler et al., 2019), but not yet for fruit powders.

With regard to process, powder composition and structure complexity, knowledge of fruit powder reconstitution is clearly insufficient in comparison with other food powders (i.e. dairy powders). Therefore, the objectives of this study were to investigate the impact of structure (compacted or non-compacted), composition (various fruits), stirring speed and material state (glassy vs rubbery depending on the $a_{w}$ ) on fruit powder reconstitution.

## 2 Material and methods

### 2.1 Fruit powders

Six industrial fruit powders of different nature were analyzed (Figure 1):

- Fruit-based powders non-compacted and compacted, denoted FNC and FC, respectively.
- Red mix powders non-compacted and compacted, denoted RNC and RC, respectively.
- Purple mix powders non-compacted and compacted, denoted PNC and PC, respectively.

Each formulation contains different mixes of fruit powders. To obtain compacted powders, each mix of non-compacted powders had undergone a compaction process to form larger
particles. Therefore, for one similar chemical composition, two powders were studied: noncompacted (NC) and compacted (C).

### 2.2 Storage conditions

All the powders were stored at two conditions that are $a_{w} \sim 0$ and $a_{w} \sim 0.35$ before using them for experiments. In order to maintain a low water activity (i.e. $a_{w} \sim 0$ ) and prevent powder caking, powders were stored at $20^{\circ} \mathrm{C}$ in a desiccator (Nalgene cabinets) containing phosphorus pentoxide ( $\mathrm{P}_{2} \mathrm{O}_{5}$ from Sigma Aldrich) as drying agent. For the second condition, powders were stored at $20^{\circ} \mathrm{C}$ in another desiccator containing magnesium chloride salts ( $\mathrm{MgCl}_{2}$ from Sigma Aldrich) to maintain an $a_{w} \sim 0.35$, in order to mimic ambient conditions. The value of water activity was often verified and determined using a Hygropalm HP23-AW (Omni Instruments, UK) before using the powders for experiments. This device, calibrated using salts whose water activity is known, has a measuring range equals 0 to 1 with an accuracy of $\pm 0.008$, over a temperature range comprised between $-10{ }^{\circ} \mathrm{C}$ and $60^{\circ} \mathrm{C}$. A sample of powder (typically around 15 g ) was poured into a polypropylene container, and the water activity measurements were realized using an electrolytic sensor. Three repetitions were performed for each sample.

### 2.3 Surface properties

### 2.3.1 Optical imaging

The influence of water activity on visual properties was evaluated with classical imaging. Pictures of the fruit powders studied were taken with a classic camera. Pictures with an optic microscope (Dinolite, 5 Megapixel Edge sensor, 10 - 200× magnification, polarizer and flexible LED control) were also recorded.

### 2.3.2 Scanning Electron Microscopy

A high-resolution field-emission scanning electron microscope (SEM) type JEOL JSM-7100F supplied with a hot (Schottky) electrongun (JEOL Ltd., Tokyo, Japan) and having a resolution around 1 nm at 30 kV was used to investigate the surface morphology and topography of fruit powders at two different water activity values. The equipment was operated at 1 kV . Samples were mounted onto SEM stubs by fixing them on a carbon double-sided adhesive tape. Finally, a coating of iridium was applied to the samples until reaching around 10 nm coating thickness.

### 2.3.3 Atomic force microscopy (AFM)

Prior to AFM experiments, fruit powders were glued onto the surface of circular glass. The surface topography of fruit powder particles was probed in air with a MFP3D-BIO instrument (Asylum Research Technology, Oxford Instrument, Manheim, Germany) using gold coated AFM-tips (NPG, Bruker SAS, Palaiseau France). The used scan area was $10 \mu \mathrm{~m} \times 10 \mu \mathrm{~m}$ (corresponding to 512 lines). Mechanical properties of individual particles were probed at the nanoscale by AFM nanoindentation technique. Measurements were performed in air and at room temperature with stiff cantilevers (MPP-13100 with $200 \mathrm{~N} / \mathrm{m}$ spring constant). The cantilever was calibrated onto sapphire substrate. The force-distance curves recorded by AFM were analyzed according to the theoretical Sneddon model to extract the mechanical properties (e.g. elasticity).

### 2.3.4 X-ray photoelectron spectroscopy

The elemental surface composition of FNC and FC (up to 10 nm depth) was measured by Xray Photoelectron Spectroscopy (XPS) (Gaiani, 2006; Rouxhet et al., 2008). Before analysis,
the samples were outgassed under vacuum for 24 h . Spectra were obtained using a KRATOS Axis Ultra X-ray photoelectron spectrometer (Kratos Analytical, Manchester, UK) equipped with a mono-chromatic Al Ka X-ray ( $h v=1486.6 \mathrm{eV}$ ) operated at 150 W . The analysis area equaled $700 \mu \mathrm{~m} \times 300 \mu \mathrm{~m}$ and spectra were collected at normal take-off angle $90^{\circ}$. Four repetitions were performed for each sample.

### 2.4 Physical and chemical properties

### 2.4.1 Differential scanning calorimetry

Differential scanning calorimetry (DSC 2500, Discovery DSC Series, TA Instruments) measurements were used to investigate the glass transition in fruit powders. Samples of powder, pre-weighed (around 10 mg ), were sealed in Tzero aluminum hermetic pans with a mechanical crimp. These pans were placed in parallel to an empty capsule, which was the reference. The samples were under protective nitrogen and the procedure was fixed to perform a first round of heating from $-20^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$ at $10^{\circ} \mathrm{C} \cdot \mathrm{min}^{-1}$ rate, followed by a cooling from $50^{\circ} \mathrm{C}$ to $-20^{\circ} \mathrm{C}$ at the same rate. A second heating from $-20^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$ at $10^{\circ} \mathrm{C} \cdot \mathrm{min}^{-1}$ rate was then performed, and the glass transition temperature ( $\mathrm{T}_{\mathrm{g}}$ ) extracted from this heating were studied. Two repetitions at least were performed for each sample.

### 2.4.2 Particle size distribution

The particle size distribution was obtained using a laser diffraction granulometer (Mastersizer 3000, Malvern Instruments, UK) equipped with Aero $S$ dry powder dispersion unit. All samples were dispersed at 1 bar air pressure. The feed rate and the hopper length values were adjusted to obtain a correct obscuration between 1 and $15 \%$. The particle size distribution was calculated from Mie theory, and provided as a volume density function. The particle size estimator was the $d_{50}$, which means that $50 \%$ of particles have a lower diameter. The span value was used as a polydispersity indicator, and is given by:

Equation 1

$$
\operatorname{span}=\frac{d_{90}-d_{10}}{d_{50}}
$$

where $10 \%, 50 \%$ and $90 \%$ of the sample particles are smaller than the diameter $d_{10}, d_{50}$ and $d_{90}$, respectively. Three repetitions were performed for each sample.

### 2.5 Reconstitution properties

2.5.1 Conductivity measurements during reconstitution

The time evolution of the conductivity was obtained using a portable conductivity S7 Standard Kit with a sensor (INLAB 738 ISM from Mettler Toledo Seven2Go). The calibration of the sensor was made at $\mathrm{T}=25^{\circ} \mathrm{C}$ with a calibration liquid at a conductivity $1413 \mu \mathrm{~S} . \mathrm{cm}^{-1}$. The time duration of the measurement was adapted depending on the sample. Conductivity measurements were realized in a beaker of 200 mL that was put in water bath with circulating water supply in order to have a constant and fixed temperature $\left(25^{\circ} \mathrm{C}\right)$. A volume of 100 mL of water was poured into the beaker and the powders were reconstituted under specific TS conditions ( $10 \pm 0.1 \mathrm{~g}$ ). The powders were blended into water, thanks to a bar magnet of length 3 cm , with a magnetic stirrer in a range of stirring speed values (from 800 to 1500 $\mathrm{rpm})$. Three repetitions were performed for each sample.

### 2.5.2 Particle size distribution during reconstitution

The particle size during reconstitution was followed using the laser diffraction granulometer (Mastersizer 3000, Malvern Instruments, UK) equipped with the Hydro MV unit. The particles were dispersed in 120 mL dispersant volume with a stirrer ( $0-3500 \pm 10 \mathrm{rpm}$ ). The dispersant used was distilled water. The samples passed through a measuring cell using a centrifugal pump (flow rate $Q=0-2 \mathrm{~L}_{\mathrm{min}}{ }^{-1}$ ). The particle size was probed with a sequential combination of measurements with red and blue light sources. Experiments were conducted with powders stored at $a_{w} \sim 0$ and $a_{w} \sim 0.35$. The stirring speed was fixed at 2000 rpm , and
water temperature at $\mathrm{T}=24 \pm 2^{\circ} \mathrm{C}$. For one measurement, the integration time of each light source was adapted depending on the sample and its kinetics (typically between 1 and 5 sec) in order to have reliable and repeatable results. The time variation of particle size distributions was assessed choosing the number of measurements and the delay between each one, depending on the sample. The mass of the studied samples, typically between 0.02 and 0.30 mg , were adapted to obtain obscuration between 1 and $30 \%$ depending on the particle size. For instance, the mass of powder rehydrated into the device was chosen at $\mathrm{m}=$ 0.15 g and $\mathrm{m}=0.30 \mathrm{~g}$ for FNC and FC, respectively. Two repetitions were performed for each sample.

## 3 Results and discussion

### 3.1 Particle size, shape and visual aspects

The particle size distributions of the six fruit powders (three fruit compositions and two structures per composition) were measured at two water activity values (Figure 2). Information related to these functions such as the mean diameter $d_{50}$, the span value and the percentage increase of $d_{50}$ between two $a_{w}$ values are presented in Table 1. Visual/optic microscopy and electronic microscopy images are presented in Figures 3 and 4, respectively. Impact of compaction. The compaction process leads systematically to a high mean diameter, and also produces only monodisperse population of particles even if the non-compacted powder has bimodal distribution (for instance, FNC/FNC and RNC/RC powders). From images, non-compacted powders seem to have a particle size around a hundred microns, which was confirmed by the determination of the $d_{50}$. Also, compaction process seems to produce more
homogeneous size distribution (images), which is confirmed by a smaller span value. Finally, images suggest that compaction process led to angular shapes particles with high rugosity. Impact of water activity. From size measurements, increasing the water activity value leads to an increase of the mean diameter, and a decrease in span value. This can be explained by the apparition of two populations: the lowest size population represents the increase in mean diameter with increasing $a_{w}$, while the higher size population (around $d \sim 1000 \mu \mathrm{~m}$ ) is due to the agglomeration of individual particles. An increase in moisture content leading to an increase in free volume due to the formation of hydrogen bonds may also impact the particle size (Jadhav et al., 2009; Moghbeli et al., 2019). The non-compacted powders are much more sensitive to the impact of water activity regarding their mean diameter, in comparison with the compacted ones as shown by the percentage increase of $d_{50}$. Moreover, for compacted powders, the greater the diameter at $a_{w} \sim 0$, the less it increases with increasing $a_{w}$. Images suggest a smoother surface at $a_{w} \sim 0.35$, in comparison with the angular shape observed at $a_{w} \sim 0$. This suggests a sticky surface that may explain the agglomerates for non-compacted powders, and a change in powder surface. Increasing water activity value seems to change the powder surface and the particle size (Liu et al., 2010). Although it is not visible using SEM imaging due to the coating, this could also change the porosity at the surface of the particles, and thus influencing the reconstitution properties (entrance of water into the structure). Finally, optical images also show a clear difference in color when increasing the water activity value, in agreement with Jiang et al. (Jiang et al., 2013). These pictures suggest a change in surface properties between $a_{w} \sim 0$ and $a_{w} \sim 0.35$, that may impact later the reconstitution by clogging pores where water could penetrate. This aspect will be discussed later in the results and discussion part.

### 3.2 Powder surface characterization

Impact of compaction. XPS analysis was performed on FNC and FC in order to evaluate the impact of the compaction process on the surface composition for powders having similar bulk composition. Three common chemical elements were detected at the surface of the powders: carbon C , oxygen O , nitrogen N with mineral traces ( K and P ). The detection of nitrogen suggests the presence of proteins at the surface. For FNC powder, minor elements were detected in very low concentration: potassium K and phosphorus P (Figure 5a). Regarding the results of the surface atomic concentration of chemical elements, there is no impact of the compaction process on the surface composition of the studied powders. Moreover, the analysis of carbon bonds (Figure 5b) reveals again no significant influence of the compaction process on the carbon element. Almost the same atomic concentration of $\mathrm{C}-\mathrm{C}$ bonds and $\mathrm{C}-\mathrm{O}$ bonds (50 \% - $50 \%$ ) is observed. This suggests that fruit powder surfaces are mainly composed of polysaccharides. Ratios between carbon element and oxygen element, and C-C bonds and other C bonds ( $\mathrm{C}-\mathrm{O}, \mathrm{C}=\mathrm{O}, \mathrm{O}-\mathrm{C}=\mathrm{O}$ ) were calculated (Figure 5 c ). These ratios give information about the hydrophilic/ hydrophobic nature of the powder surface. It appears that the surface is mostly similar and that the compaction had no impact measured by XPS. The XPS results suggested that potential differences in reconstitution properties should not come from a chemical point of view in term of surface composition (Nijdam and Langrish, 2006; Murrieta-Pazos et al., 2012).

Impact of water activity. To go further and quantify the impact of water activity on the surface of fruit powders, surface topography and nanomechanics were performed by AFM (Figure 6). Regarding the measurements at $a_{w} \sim 0.35$, it was very difficult to keep the contact between the AFM tip and the surface, probably due to a thin layer of water present at the surface as already reported in literature (Eaton and West, 2010). For nanoindentation, it can be seen
that the distribution is centered at 10 MPa for the powders stored at $a_{w} \sim 0$ and a shift to lower values ( 5 MPa ) was observed for the powders stored at $a_{w} \sim 0.35$. This means that powders stored at higher water activity present a softer surface compared to the ones stored at $a_{w} \sim 0$. The elasticity maps reveal that some regions are stiffer than the rest of the surface meaning that nanomechanical properties are inhomogeneous at the particle surface. It appears that increasing water activity impacts the surface properties of powders. DSC measurements were obtained for the six fruit powders studied at two $a_{w}$, in order to determine the influence of water activity on the glass transition temperature evolution (Table 2). For all powders, a glass transition clearly appeared and the endpoint glass transition temperature $\left(\mathrm{T}_{\mathrm{g}}\right)$ was extracted. From a general point of view, glass transition occurred at lower temperature for non-compacted powders than for compacted ones. This result may be due to both an increase in surrounding pressure and a decrease in water content as already reported in literature (Jadhav et al., 2009; Lopez-Quiroga et al., 2019; Moghbeli et al., 2019). Furthermore, a significant decrease of the glass transition temperature $\mathrm{T}_{\mathrm{g}}$ was observed with increasing water activity value, which could be explained by an increase in free volume (Roos, 2002). The most important result is that all powders (whatever the compaction and the relative activity) are above or slightly below their glass transition at ambient temperature $\left(\mathrm{T}=20^{\circ} \mathrm{C}\right)$. At $\mathrm{a}_{\mathrm{w}}=0$, some samples are in the glassy state (FC, PNC and PC powders) and some (FNC, RNC, RC powders) are just above Tg , leading to a transition from a glassy state to a rubbery state. As these samples are close to the transition from glassy to rubbery state, in these conditions, at microscopic scale the matrix is partly at rubbery and partly at glassy state. At $\mathrm{a}_{\mathrm{w}}=0.35$, all samples are at the rubbery state. Also, for material containing sugars, like fruit powders, this transition from brittle solids to sticky materials is responsible for caking and particle size increase as previously observed by visual and microscopy images.

Therefore, powders at $a_{w} \sim 0.35$ are under a rubbery state whereas the one maintained at low $a_{w}$ are partly under a glassy state. As seen in Figures 3 and 4 and already discussed, particle surface is rougher and more angular at $a_{w} \sim 0$. It confirms that a material transition occurred; this transition being correlated to a modification of the nanomechanical properties at the particle surface. These surface changes should influence the reconstitution, particularly concerning the initial interaction between particle and water, during the wetting and swelling steps.

### 3.3 Powders reconstitution ability

Conductivity measurements. The conductivity values were followed with time during reconstitution of the six studied powders at a water activity $\sim 0$ and $\sim 0.35$ (Figure 7). An example of the typical time evolution of the conductivity and the extraction of the reconstitution time $\left(\tau_{R}\right)$ are plotted in Supplementary material 1 . The conductivity value quickly increases and then reaches a constant value. The reconstitution time was then evaluated by considering that the reconstitution is reached when the conductivity value equals $90 \%$ of the maximum conductivity value (Mitchell et al., 2015, 2019).

The non-compacted powders have systematically faster reconstitution than the compacted ones, thus resulting in shorter reconstitution times. This is mainly due to the particle size, which is higher for the compacted powder and add a step of disintegration of the granules. However, two distinct behaviors appear concerning the evolution of $\tau_{R}$ with shear, which seems to depend on the water activity value. At low water activity, the evolution of $\tau_{R}$ with the stirring speed, obtained by conductivity measurements, exhibits that an increase in stirring speed leads to a decrease of $\tau_{R}$. This comes from a better water entrance through particle surface porosity and therefore a faster reconstitution of particles under applied
shear. This result is usually observed by authors for food powders and more particularly for dairy powders (Andre et al., 2012). But at a higher water activity ( $\sim 0.35$ ), the behavior during reconstitution is significantly and systematically changed. Although reconstitution times are higher for compacted powders than for non-compacted, $\tau_{R}$ does not evolve significantly with shear for a given fruit powder, in the range of stirring speed studied (800-1500 rpm). Therefore, it is observed that the reconstitution of these six powders is shear dependent at low relative humidity and non-shear dependent at a higher relative humidity. This result was totally unexpected and to the best of our knowledge, it was never observed until now. This could come from the fact that powder surface at $a_{w} \sim 0.35$ is partially hydrated leading to a swelling of the particles that is reflected by the particle size increase. In that case, the limiting factor for powder reconstitution is mainly the diffusion of water inside the structure. This could also explain the observation that for some powders (FNC, RC, PNC and PC) and at low stirring speed value $(\mathrm{N}=750-800 \mathrm{rpm}), \tau_{R}$ at $a_{w} \sim 0$ is lower than $\tau_{R}$ at $a_{w} \sim 0.35$. These results clearly put in evidence that increasing water activity value leads to a non-dependence of shear on the reconstitution time, in the range of stirring speed studied.

Particle size distribution (PSD). The experiments of reconstitution by particle sizing were performed for FNC and FC powders in order to confirm the results obtained by conductivity measurements and verify the final state of the powders. The results of the time evolution of the volume density functions are presented in the form of a map with both the initial and the final PSD at $a_{w} \sim 0$ and $a_{w} \sim 0.35$ for FNC and FC (Figure 8). Although a larger particle size at the beginning when increasing the water activity, a given composition powder leads to an identical final volume density function, irrespective of the initial particle structure (compacted or non-compacted) and the water activity value. Rather, these two parameters (structure and $\left.a_{w}\right)$ influence the reconstitution time. It can also be noticed that the initial and final volume
density functions of FNC at $a_{w} \sim 0$ are almost the same, with a slight increase of the volume density for the main peak ( $d \sim 200 \mu \mathrm{~m}$ ) and a slight decrease of the secondary peak ( $d \sim 30$ $\mu \mathrm{m})$. This result suggests that mainly dispersion step occurs during reconstitution of this powder. Indeed, disintegration of small agglomerates into primary particles (from the main peak) and small particles (from secondary peak) would explain the observations. The time evolution of the mean diameter $d_{50}$ extracted from volume density functions is plotted in Figure 9. The data are well fitted to an incomplete dissolution model derived from the NoyesWhitney model (Cogswell et al., 2006). This model was proposed and successfully used by Fang et al. (Fang et al., 2011) in the case of the reconstitution of milk protein concentrate by measuring the particle size through optical images. The model is defined as:

## Equation 2

$$
d_{50}(t)=\left(d_{0}-d_{\infty}\right) \exp \left(-\frac{t}{\tau_{P S D}}\right)+d_{\infty}
$$

where $d_{0}$ is the initial mean diameter (dry case), $d_{\infty}$ is the final mean diameter (at the end of the rehydration) and $\tau_{P S D}$ is the characteristic reconstitution time of the particle size distribution. The characteristic reconstitution time and the final mean diameter value extracted are presented in Table 3. As already observed with the conductivity measurements, the compaction process increases the reconstitution time because a step of granule destruction adds up compared to non-compacted powders. The results also show that increasing the water activity value leads to an increase in reconstitution time. The results from granulometry during reconstitution provide a new piece of information: the final mean diameter depends neither on the water activity value nor the compaction process. This means that powders reach the same final state after total reconstitution.

### 3.4 Relationships between powder process, structure and function at two water activities

The relationships between process (compaction), structure (glassy/rubbery state) and function (reconstitution ability) is established with this multi-scale approach. From a macroscopic point of view, fruit powders are particularly sensitive to their storage environment (Islam et al., 2016). The observations demonstrate a transition from a glassy state to a rubbery state, easily visible by a color and aspect changes (caking due to the plasticizing effects of water on the particle surface) with the water activity increase at typical storage temperature (i.e. around $20^{\circ} \mathrm{C}$ ). The glass transition can appear either by increasing the temperature and/or the water activity (Roos, 2002). Here, a clear impact of water activity on macroscopic fruit powders characteristics was observed. It was already shown an inverse relationship between $\mathrm{T}_{\mathrm{g}}$ and water activity for fruit powders (Tonon et al., 2009; Goula and Adamopoulos, 2010; Islam et al., 2016). From a microscopic point of view, this transition from angular particles to smoother ones with a large increase in the mean diameter (swelling of particles) was observed with increasing water activity. These microscopic modifications are observed by both SEM and PSD with the calculation of the $d_{50}$ increase with relative humidity. Again, similar observations were previously made for sugar rich powders (Tonon et al., 2009; Goula and Adamopoulos, 2010; Islam et al., 2016). Finally, a transition from a stiff and brittle surface to a soft surface using nanomechanics was observed with increasing water activity value. The evolution of the Young's modulus is in agreement with both macroscopic and microscopic evolution of the powders.

It is well admitted that many factors can affect the powder reconstitution. It may be the method of reconstitution (type of stirrer, configuration, intensity of agitation, water temperature ...) (Fitzpatrick et al., 2000; Jeantet et al., 2010) or the material properties (particle size distribution, density, porosity, morphology, surface
hydrophilicity/hydrophobicity...) (Gaiani et al., 2007a; Murrieta-Pazos et al., 2012). The novelty in this study is that it has been shown that shear rate does not affect the reconstitution behavior at high water activity value ( $\sim 0.35$ ) whereas it impacts at low water activity value $(\sim 0)$. This non-dependence to shear was never observed for food powders and more particularly dairy powders largely studied at various shear rates (Richard et al., 2013). Nevertheless, the composition dairy powders is very different than fruit powders. Furthermore, the glass transition temperature of fruit powders is lower compared to milkbased powders due to high fraction of sugars. Recently, a study of Wangler et al. (Wangler et al., 2019) on the reconstitution of biopolymer powders with different coating demonstrated the importance of a viscous layer on the dissolution/non-dissolution rate. The authors showed that a biopolymer particle exhibiting a layer with low viscous cohesion reconstitutes first by capillarity and then by diffusion. On the contrary, increasing the layer thickness due to swelling leads to an entrance of the water mainly by diffusion. Regarding our results on fruit powders, an analogy can be made with reconstitution of fruit powders depending on the water activity. Indeed, mainly three reconstitution steps are relevant to our study: the wetting, the swelling and the dispersion/dissolution. The dispersion/dissolution rate mainly depends on the specific surface area in contact with water, which is higher for noncompacted powders. Thus, the effect of compaction process is very important at this reconstitution step. At $a_{w} \sim 0$, powders are under a glassy state and their porous surface help both surface erosion and the entrance of water by capillarity, following by water diffusion. In this case, increasing shear leads to a decrease of the reconstitution time. However, for particles under a rubbery state (at $a_{w} \sim 0.35$ ), the wetting/swelling steps have already begun, resulting in the collapse of the pore network, making appear a viscous layer. In this case, increasing shear does not improve water entrance due to the viscous layer on the surface of
the particles. Thus, for this elevated relative humidity, diffusion may be the limiting step, i.e. the step with which we can improve the reconstitution. In this particular case, to promote the rate of reconstitution speed it may be useful to increase the temperature to reduce the viscosity in the viscous layer rather than increasing the shear rate. The hypothesis proposed in this work is presented in a schematic in Figure 10.

## 4 Conclusion

In the present work, the reconstitution of fruit powders was evaluated. Three mixes were used in a non-compacted and a compacted state. First of all, it was found that the compaction process only delays the entire reconstitution process but the final state was identical for each mix, irrespective of the initial structure of the powder. Secondly, the crucial role of water activity was evidenced and its impact on the kinetics of powder reconstitution was evaluated. In fact, at low water activity, a shear-dependence of reconstitution kinetics was observed indicating that the increase in the stirring speed improved the entrance of water inside a particle. In that case, powders were under the glass transition temperature, so they were in the glassy state. This was evidenced by both DSC measurements and also by imaging (SEM and AFM), which reveals porous/angular shapes and stiff particles. On the contrary, at a higher water activity $(\sim 0.35)$, the powders were above the $\mathrm{T}_{\mathrm{g}}$ due to the plasticizing effect of water. The powders were in the rubbery state and the particles appeared smooth and soft. Under these circumstances, the kinetics of reconstitution was found independent of the stirring speed. This behavior may have resulted from the formation of a viscous layer at the particle surface, which is responsible for the closure of the porosity at the particle surface. The main consequence is that the entrance of water into the internal structure is significantly
reduced. Thus, diffusion becomes the rate controlling step for powder reconstitution. Hence, increasing shear rate which would typically enhance the mass transfer coefficient on the surface is not observed under these circumstances.

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Figures and Captions. and.


FC


Figure 1. Macroscopic and microscopic views of the fruit powders studied. Top: powders before compaction process (FNC, RNC and PNC). Bottom: powders after compaction process (FC, RC


Figure 2. Particle size distribution functions of the six fruit powders studied at the two water activity values ( $a_{w} \sim 0$ and $\sim 0.35$ ).




Figure 3. Pictures and microscopic images at two water activity values ( $a_{w} \sim 0$ and $\sim 0.35$ ) of the six fruit powders studied (FNC, FC, RNC, RC, PNC and PC).


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Figure 4. SEM images at various magnifications for the six fruit powders studied at both $a_{w} \sim 0$ and $a_{w} \sim 0.35$.



Figure 5. (a) Surface atomic concentration of chemical elements, (b) proportion of carbon bonds and (c) proportion of carbon bonds ratios detected at the surface of FNC and FC powders.

| Elements | FNC | FC |
| :---: | :---: | :---: |
| $\mathbf{C}_{\mathbf{1 s}}$ | $70.92 \pm 0.13$ | $73.38 \pm 1.96$ |
| $\mathbf{0}_{\mathbf{1 s}}$ | $27.05 \pm 0.18$ | $25.39 \pm 1.91$ |
| $\mathbf{N}_{\mathbf{1 s}}$ | $1.79 \pm 0.10$ | $1.23 \pm 0.12$ |
| $\mathbf{K}_{\mathbf{2} \mathbf{p}}$ | $0.15 \pm 0.03$ | -- |
| $\mathbf{P}_{\mathbf{2} \mathbf{p}}$ | $0.09 \pm 0.09$ | -- |

(a)


Figure 6. Surface topography at two water activity values for RC powder and corresponding distribution of the elastic modulus after curve fitting with the Sneddon model. Inserts in histograms represent the associated elasticity maps.




Figure 7. Evolution of the rehydration time as a function of the stirring speed value N at a fixed water temperature $\mathrm{T}=25^{\circ} \mathrm{C}$, and at different water activity values for (a) FNC and FC powders, (b) RNC and RC powders and (c) PNC and PC powders.


(a) Stirring speed (rpm)

(b)




Figure 8. At both $a_{w} \sim 0$ and $a_{w} \sim 0.35$, for (a) FNC powder and (b) FC powder. Left: Maps presenting the time evolution of the volume density function. Right: Volume density function at $t_{\text {initial }}$ (dry powder) and $t_{\text {final }}$ (powder entirely rehydrated).

(b)

Figure 9. Logarithmic plot of the time evolution of the mean diameter $d_{50}$ extracted from volume density functions for FNC and FC powders, at $a_{w} \sim 0$ and $a_{w} \sim 0.35$. The data are well fitted to equation 2 (solid lines and dotted lines).


Figure 10. Summary of the relevant results in term of physicochemical properties from macroto nano- scale for fruit powders.


|  |  | $\boldsymbol{d}_{50}(\mu \mathrm{~m})$ | span | \% increase $\boldsymbol{d}_{\mathbf{5 0}}$ with water activity |
| :---: | :---: | :---: | :---: | :---: |
| FNC | $a_{w} \sim 0$ | $152 \pm 1$ | $1.83 \pm 0.04$ | 270 \% |
|  | $a_{w} \sim 0.35$ | $563 \pm 136$ | $3.22 \pm 1.34$ |  |
| FC | $a_{w} \sim 0$ | $1330 \pm 39$ | $1.55 \pm 0.10$ | 10 \% |
|  | $a_{w} \sim 0.35$ | $1460 \pm 148$ | $1.26 \pm 0.30$ |  |
| RNC | $a_{w} \sim 0$ | $387 \pm 46$ | $3.36 \pm 0.77$ | 98 \% |
|  | $a_{w} \sim 0.35$ | $765 \pm 3$ | $2.30 \pm 0.09$ |  |
| RC | $a_{w} \sim 0$ | $671 \pm 33$ | $2.17 \pm 0.24$ | 59 \% |
|  | $a_{w} \sim 0.35$ | $1070 \pm 53$ | $1.49 \pm 0.18$ |  |
| PNC | $a_{w} \sim 0$ | $348 \pm 17$ | $3.12 \pm 0.41$ | 121 \% |
|  | $a_{w} \sim 0.35$ | $770 \pm 18$ | $2.38 \pm 0.07$ |  |
| PC | $a_{w} \sim 0$ | $634 \pm 31$ | $2.55 \pm 0.18$ | 74 \% |
|  | $a_{w} \sim 0.35$ | $1100 \pm 69$ | $1.54 \pm 0.21$ |  |

Table of content

Table 1. Information related to particle size distribution functions of the six fruit powders studied at $a_{w} \sim 0$ and $a_{w} \sim 0.35$.

Table 2. Endpoint glass transition temperatures $T_{g}\left({ }^{\circ} \mathrm{C}\right)$ of the six fruit powders studied during the second heat rate, at $a_{w} \sim 0$ and $a_{w} \sim 0.35$.

|  | FNC | FC | RNC | RC | PNC | PC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 14.55 | 24.92 | 13.91 | 17.71 | 26.53 | 24.73 |
| $a_{w} \sim 0$ | $\pm 0.18$ | $\pm 0.44$ | $\pm 0.14$ | $\pm 0.54$ | $\pm 1.98$ | $\pm 1.67$ |
|  | -1.77 | -0.52 | -4.96 | -2.80 | 1.91 | -4.28 |
| $a_{w} \sim 0.35$ | $\pm 1.64$ | $\pm 1.02$ | $\pm 1.85$ | $\pm 1.02$ | $\pm 1.00$ | $\pm 1.16$ |

Table 3. Parameters values extracted from exponential time decay functions (Equation 2) for FNC and FC at $a_{w} \sim 0$ and $a_{w} \sim 0.35$ : characteristic PSD rehydration time $\tau_{P S D}$ and final mean diameter value $d_{\infty}$.

|  |  | $\boldsymbol{\tau}_{\text {PSD }}(\boldsymbol{s})$ | $\boldsymbol{d}_{\infty}(\mu \mathrm{m})$ |
| :---: | :---: | :---: | :---: |
| FNC | $a_{w} \sim 0$ | $2.35 \pm 0.09$ | $177 \pm 7$ |
|  | $a_{w} \sim 0.35$ | $4.76 \pm 0.21$ | $175 \pm 8$ |
|  | $a_{w} \sim 0$ | $13.27 \pm 0.01$ | $178 \pm 1$ |
|  | $a_{w} \sim 0.35$ | $17.57 \pm 0.45$ | $171 \pm 5$ |

