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# Energy variation and stress fields of spherical inclusions with eigenstrain in three-dimensional anisotropic bi-materials

T. Richeton<sup>a,\*</sup>

<sup>a</sup>*Université de Lorraine, CNRS, Arts et Métiers, LEM3, F-57000 Metz, France*

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## Abstract

In this study, expressions for the interior stress fields of a spherical inclusion with uniform eigenstrain embedded in an anisotropic bi-material featuring a planar interface are derived. These expressions involve surface integrals of the imaginary term of the first derivative of the Green tensor in an anisotropic bi-material which are well-suited for standard numerical integrations. Specific formulations are provided for cases where the inclusion belongs to either the same material or both materials. Additionally, expressions are presented for the equivalent Eshelby tensor. The interior stress fields and variations in elastic strain energy are computed using cubic elastic constants of Cu. Various inclusion positions relative to the interface, eigenstrain forms, and crystallographic orientations are considered. Notably, stress variations within the inclusion are not necessarily monotonous. For instances involving dilatational eigenstrain, the elastic strain energy variation may exhibit multiple extrema. The global minimum and maximum consistently occur when the inclusion spans both materials. In the context of symmetrical tilt boundaries, energy variations are perfectly symmetric, with a global minimum on the interface that decreases with the tilt angle. The significance of the observed energy variations for defects segregation is quantitatively assessed by comparing them with the interaction energy between an eigenstrain and a grain boundary stress field.

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\*Corresponding author.

*Email address:* `thiebaud.richeton@univ-lorraine.fr` (T. Richeton)

*Keywords:* Inclusions, Interface, Anisotropic elasticity, Green function, Image force

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## 1. Introduction

The study of elastic fields generated by inclusions within an elastic matrix stands as a cornerstone in micromechanics, significantly influencing the development of advanced multi-components alloys (Mura, 1987; Zhou, 2013; Barnett and Cai, 2018). An inclusion is associated with an eigenstrain, representing the stress-free strain the inclusion would have if removed from the encompassing matrix (Mura, 1987; Barnett and Cai, 2018). Inclusions are generally considered in an infinite homogeneous medium as in the pioneering work of Eshelby (1957). However, many works also focus on inclusion problems within finite spaces (e.g., (Eshelby, 1954, 1961; Kinoshita and Mura, 1984; Li et al., 2007)) and half-spaces (e.g., (Mindlin and Cheng, 1950; Chiu, 1978; Seo and Mura, 1979; Pan and Yang, 2001)), necessitating the introduction of ‘image’ terms, i.e. terms that should be added to the elastic fields of the infinite medium in order to satisfy the boundary conditions at outer surfaces. Despite this extensive exploration, limited attention is given to inclusions in bi-materials, which also demand consideration of ‘image’ terms. Existing studies typically focus on dissimilar isotropic elastic solids (Bacon, 1972; Gladwell, 1999; Selvadurai, 2000; Franciosi and Charles, 2016) and/or plane or anti-plane problems (Zhang and Chou, 1985; Ru, 2001; Ru et al., 2001; Jiang and Pan, 2004; Wang et al., 2007). Yet, the 3D problem of an inclusion embedded in an anisotropic bi-material holds potential significance in various applications, such as assessing the strength of laminated materials with reinforcements or better understanding the segregation at interfaces of defects like solute atoms, vacancies, precipitates (oxydes, carbides, etc.) or voids. In particular, solute atom segregation to grain boundaries markedly influences material properties, including grain boundary energy, mobility and cohesion (Dingreville and Berbenni, 2016). Solute atoms can be treated as spherical misfitting inclusions with purely dilatational eigenstrain (White and Coghlan, 1977; Cai et al., 2014; Dingreville and Berbenni, 2016). Point defects like vacancies and solute atoms (in substitution or in insertion) can also be modeled as a distribution of point-forces, i.e. like a force multipole that mimics the forces imposed on the atoms surrounding the defects (Siems, 1968; Bacon et al., 1980; Balluffi, 2016; Clouet et al., 2018). While this representation is actually only valid outside the defect, it becomes particularly

relevant when considering the interaction energy with an external strain field. For instance, it is demonstrated that representing the defect with the first moment of the point force distribution, known as the elastic dipole, is equivalent to considering a uniform eigenstrain within a small inclusion but only in regions far from the inclusion (Clouet et al., 2018). The elastic dipole tensor can also be related to the displacement dipole tensor, which quantifies the strength of the point defect (Lazar, 2017). In the latter approach, the point defect is modeled with a three-dimensional Dirac  $\delta$ -singularity in the eigenstrain tensor such that only average stress values can be defined at the defect position due to the Dirac core (Lazar, 2017). Consequently, the representation of a defect with a dipole tensor cannot capture the full complexity of the interaction energy between a defect and an interface, as the interior stress fields of an inclusion within a bi-material are necessarily non-uniform (see, e.g., (Seo and Mura, 1979)), whereas a finite inclusion may also spans both materials.

The current study deals with the issue of an inclusion of finite size embedded in a bi-material considering linear heterogeneous anisotropic elasticity (see Fig.1). As explained, the interface introduces modifications to the elastic fields within and surrounding the inclusion compared to the infinite medium. The gradient of the change in elastic strain energy associated with the defect manifests as a force on the defect itself, known as an image force. This configurational force, exhibiting either an attractive or repulsive nature, depends on the defect's position relative to the interface. It is known that a softer material will attract the defect (whether it is a dislocation or a point defect), while a harder one will repel it. This is rooted in the fact that the elastic distortions induced by the defect yield lower contributions to the elastic strain energy when situated within the softer material. However, the scenario becomes more intricate when considering a grain boundary that separates two crystals of the same material but with different orientations. In addition, the details of how the elastic strain energy varies as the inclusion is continuously displaced from one material to another remain unexplored.

The stress fields and elastic strain energy variations for an inclusion within a bi-material can be effectively computed using the anisotropic elastic Green functions in a bi-material with a planar interface, as developed by Pan and Yuan (2000), and combining them with the Green's function formulation for the inclusion stress fields (Mura, 1987). The expression of the anisotropic elastic Green functions in a bi-material were derived via the Stroh formalism (Stroh, 1958, 1962) and the 2D Fourier transform method. They encom-

pass the full-space Green’s tensor and an additional complementary part. The latter can be efficiently computed through a regular line-integral over the range  $[0, \pi]$ , amenable to standard numerical integration methods (Pan and Yuan, 2000; Chu et al., 2011, 2012).

The paper is organized as follows. Section 2 presents the theoretical framework. The expressions of the stress field due to a distribution of eigenstrains in a general (i.e. homogeneous or heterogeneous) infinite elastic medium are first introduced. Then, particular expressions of the stress fields are derived considering a uniform eigenstrain within a spherical inclusion in a bi-material, whether it belongs to a single material or spans both materials (see Fig.1). Furthermore, the expression for the elastic strain energy is provided, along with simplifications emerging from the assumption of cubic elasticity and dilatational eigenstrain. In Section 3, a convergence study is undertaken regarding the numerical integrations involved in the computation of the elastic strain energy. Additionally, a comparative analysis with the known energy variation in an isotropic half-space is performed, ensuring the robustness of the numerical implementation. Moving on to Section 4, the results in terms of interior stress fields profiles and variations in elastic strain energy are shown assuming cubic elastic constants of Cu. Various inclusion positions relative to the interface, diverse forms of eigenstrain, and distinct crystallographic orientations are explored. Section 5 engages in a thorough discussion of these results, with a specific focus on quantitatively assessing the significance of the image effect. This assessment is made through comparisons with the interaction energy between an eigenstrain and an external stress field, such as the one arising from a grain boundary. Summarizing remarks follow in Section 6.

Throughout the paper, bold letters are used for vectors, tensors and matrices. The superscript T denotes the transpose of a matrix and an overbar the conjugate of a complex function. The Einstein convention over repeated indices is used.  $i$  denotes the imaginary unit.

## 2. Theoretical framework

We consider an infinite general (i.e. homogeneous or heterogeneous) elastic medium of volume  $V$  and a distribution of eigenstrains  $\boldsymbol{\varepsilon}^*$ . In the absence of body force, the displacement vector  $\mathbf{u}$  follows the Navier equation

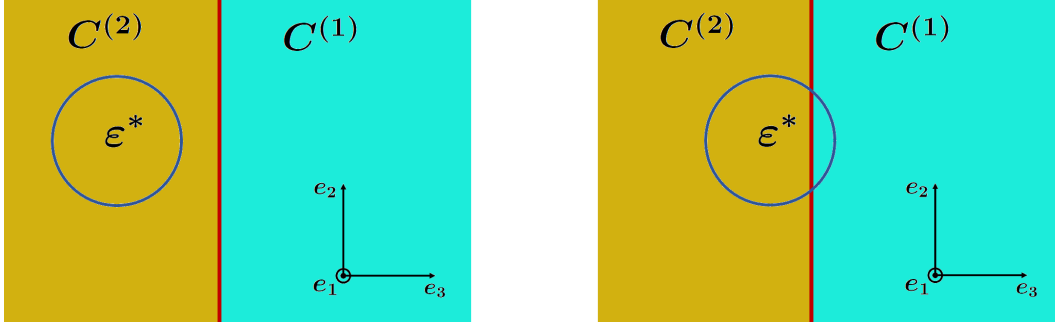


Figure 1: Infinite bi-material made of material (1) characterized by elasticity tensor  $\mathbf{C}^{(1)}$  in the region  $x_3 > 0$  and of material (2) characterized by  $\mathbf{C}^{(2)}$  in the region  $x_3 < 0$ . On the left, the spherical inclusion with a uniform eigenstrain  $\boldsymbol{\varepsilon}^*$  belongs only to material (2). On the right, the inclusion spans the two materials.

$$C_{ijkl}(\mathbf{x}) \frac{\partial u_k(\mathbf{x})}{\partial x_l \partial x_j} = C_{ijkl}(\mathbf{x}) \frac{\partial \varepsilon_{kl}^*(\mathbf{x})}{\partial x_j} \quad (1)$$

where  $\mathbf{C}$  is the fourth-rank tensor of anisotropic elastic constants that possesses the symmetries  $C_{ijkl} = C_{klij} = C_{jikl} = C_{ijlk}$ .  $\mathbf{x}$  denotes a particular point of  $V$  and the indices refer to a rectangular Cartesian frame  $(\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$ . The elastic Green tensor  $\mathbf{G}$  of the Navier equation is defined by (Barnett, 1972; Mura, 1987; Lazar, 2016, 2017)

$$C_{ijkl}(\mathbf{x}) \frac{\partial G_{km}}{\partial x_l \partial x_j}(\mathbf{x}, \mathbf{y}) + \delta_{im} \delta(\mathbf{x} - \mathbf{y}) = 0 \quad (2)$$

$\delta_{im}$  is the Kronecker delta tensor and  $\delta(\mathbf{x} - \mathbf{y})$  is the three-dimensional Dirac delta function. The Green's function  $G_{ij}(\mathbf{x}, \mathbf{y})$  represents the elastic displacement in the  $\mathbf{e}_i$  direction at point  $\mathbf{x}$  induced by a unit force in the  $\mathbf{e}_j$  direction applied at point  $\mathbf{y}$  (Mura, 1987; Barnett, 1972). For a distribution of eigenstrains, it satisfies the equation (Mura, 1987)

$$u_i(\mathbf{x}) = - \int_V G_{ij}(\mathbf{x}, \mathbf{y}) C_{jlmn}(\mathbf{y}) \frac{\partial \varepsilon_{mn}^*(\mathbf{y})}{\partial y_l} d\mathbf{y} \quad (3)$$

where the term  $-C_{jlmn}(\mathbf{y}) \frac{\partial \varepsilon_{mn}^*(\mathbf{y})}{\partial y_l}$  represents a fictitious body force in the  $\mathbf{e}_j$  direction. By integration by parts and assuming the boundary terms vanish, we have (Mura, 1987)

$$u_i(\mathbf{x}) = \int_V C_{jlmn} \varepsilon_{mn}^*(\mathbf{y}) \frac{\partial G_{ij}(\mathbf{x}, \mathbf{y})}{\partial y_l} d\mathbf{y} \quad (4)$$

Hence, from Hooke's law, the stress field due to a distribution of eigenstrains in a general infinite elastic medium may be expressed as

$$\sigma_{pq}(\mathbf{x}) = C_{pqim}(\mathbf{x}) \left( \int_V C_{jklm}(\mathbf{y}) \varepsilon_{ln}^*(\mathbf{y}) \frac{\partial G_{ij}}{\partial y_k \partial x_m}(\mathbf{x}, \mathbf{y}) d\mathbf{y} - \varepsilon_{im}^*(\mathbf{x}) \right) \quad (5)$$

### 2.1. Homogeneous medium

For an infinite homogeneous body, we introduce  $\mathbf{G}^\infty$  as the full-space anisotropic elastic Green tensor. We have then  $\frac{\partial G_{ij}^\infty}{\partial y_l}(\mathbf{x}, \mathbf{y}) = -\frac{\partial G_{ij}^\infty}{\partial x_l}(\mathbf{x}, \mathbf{y})$  (Mura, 1987), and thus the more classical expression of the stress field for a distribution of eigenstrains is retrieved

$$\sigma_{pq}(\mathbf{x}) = -C_{pqim} \left( \int_V C_{jklm} \varepsilon_{ln}^*(\mathbf{y}) \frac{\partial G_{ij}^\infty}{\partial x_k \partial x_m}(\mathbf{x}, \mathbf{y}) d\mathbf{y} + \varepsilon_{im}^*(\mathbf{x}) \right) \quad (6)$$

### 2.2. Bi-material

We now consider an infinite bi-material made of material (1) characterized by elasticity tensor  $\mathbf{C}^{(1)}$  in the region  $x_3 > 0$  and of material (2) characterized by  $\mathbf{C}^{(2)}$  in the region  $x_3 < 0$ . The two materials are thus separated by a planar interface whose normal is along  $\mathbf{e}_3$ . The latter is assumed perfectly bonded. From Eq. 5, the stress field due to a distribution of eigenstrains can be written as

$$\sigma_{pq}(\mathbf{x}) = C_{pqim}(\mathbf{x}) \left( \int_V C_{jklm}(\mathbf{y}) \varepsilon_{ln}^*(\mathbf{y}) \frac{\partial G_{ij}^{Bi}}{\partial y_k \partial x_m}(\mathbf{x}, \mathbf{y}) d\mathbf{y} - \varepsilon_{im}^*(\mathbf{x}) \right) \quad (7)$$

where  $\mathbf{G}^{Bi}$  is the 3D anisotropic elastic Green tensor which was derived by Pan and Yuan (2000). For such a bi-material, it is noteworthy that the derivative relationship is lost,  $\frac{\partial G_{ij}^{Bi}}{\partial y_l}(\mathbf{x}, \mathbf{y}) \neq -\frac{\partial G_{ij}^{Bi}}{\partial x_l}(\mathbf{x}, \mathbf{y})$ , as well as the symmetry relations,  $G_{ij}^{Bi}(\mathbf{x}, \mathbf{y}) \neq G_{ji}^{Bi}(\mathbf{x}, \mathbf{y})$  (Chu et al., 2012).

In the present work, we write  $\mathbf{G}^{Bi}$  as the sum of a full-space term and an imaginary term  $\mathbf{G}^{Im}$  as follows

$$G_{ij}^{Bi}(\mathbf{x}, \mathbf{y}) = \begin{cases} G_{ij}^{\infty(1)}(\mathbf{x}, \mathbf{y}) + G_{ij}^{Im}(\mathbf{x}, \mathbf{y}) & \text{if } x_3 > 0 \\ G_{ij}^{\infty(2)}(\mathbf{x}, \mathbf{y}) + G_{ij}^{Im}(\mathbf{x}, \mathbf{y}) & \text{if } x_3 < 0 \end{cases} \quad (8)$$

The expressions of  $\mathbf{G}^{Im}$  depend on the signs of  $x_3$  and  $y_3$  (Pan and Yuan, 2000; Chu et al., 2011, 2012). They are explicitly given in the Appendix B.

### 2.2.1. Uniform eigenstrain within a spherical inclusion belonging to a same material

In the following, the problem is further restricted to the issue of a uniform eigenstrain  $\boldsymbol{\varepsilon}^*$  within a spherical inclusion of radius  $R$  and volume  $V^I$ . If the whole inclusion completely belongs to a same material, then the stress field inside the spherical inclusion writes

$$\sigma_{pq}(\mathbf{x}) = C_{pqim}(\mathbf{x}) \left( C_{jklm}(\mathbf{x}) \varepsilon_{ln}^* \left( E_{ijkm}(\mathbf{x}) + \int_{V^I} \frac{\partial G_{ij}^{Im}}{\partial y_k \partial x_m}(\mathbf{x}, \mathbf{y}) d\mathbf{y} \right) - \varepsilon_{im}^* \right) \quad (9)$$

where the fourth-rank tensor  $\mathbf{E}$  is defined as (Kröner, 1990; Lazar, 2016)

$$E_{ijkm}(\mathbf{x}) = \begin{cases} E_{ijkm}^{(1)} = - \int_{V^I} \frac{\partial G_{ij}^{\infty(1)}}{\partial x_k \partial x_m}(\mathbf{x}, \mathbf{y}) d\mathbf{y} & \text{if } x_3 > 0 \\ E_{ijkm}^{(2)} = - \int_{V^I} \frac{\partial G_{ij}^{\infty(2)}}{\partial x_k \partial x_m}(\mathbf{x}, \mathbf{y}) d\mathbf{y} & \text{if } x_3 < 0 \end{cases} \quad (10)$$

$\mathbf{E}$  is related to the Dirac  $\delta(\mathbf{x} - \mathbf{y})$ -term of the second derivative of the full-space Green tensor (Lazar, 2016). It can be computed almost instantaneously via an integral over the unit sphere (Kneer, 1965; Lazar, 2016) (see details in the Appendix A).

Using Gauss's theorem, the volume integral term is reduced to a surface integral

$$\sigma_{pq}(\mathbf{x}) = C_{pqim}(\mathbf{x}) \left( C_{jklm}(\mathbf{x}) \varepsilon_{ln}^* \left( E_{ijkm}(\mathbf{x}) + \int_{\partial V^I} \frac{\partial G_{ij}^{Im}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right) - \varepsilon_{im}^* \right) \quad (11)$$



$\partial V^I$  denotes the surface of the spherical inclusion and  $\mathbf{n}$  its external unit normal. It must be underlined that the introduction of the tensor  $\mathbf{E}$  and its computation from Eq. A.4 is essential from a numerical point of view. Otherwise, the numerical satisfaction with a good accuracy of Eq. 10 is very slow to achieve.

From Eq. 11, one may also define the Eshelby tensor for a spherical inclusion in a bi-material,  $\mathbf{S}^{Esh, Bi}$ . The latter should connect the total strain with the eigenstrain,  $\varepsilon_{im} = S_{imln}^{Esh, Bi} \varepsilon_{ln}^*$  and should possess the symmetries  $S_{imln}^{Esh, Bi} = S_{miln}^{Esh, Bi} = S_{imnl}^{Esh, Bi}$ . Hence, we might define

$$\begin{aligned} S_{imln}^{Esh, Bi}(\mathbf{x}) &= \frac{1}{2} C_{jklm}(\mathbf{x}) (E_{ijkm}(\mathbf{x}) + E_{mjki}(\mathbf{x})) \\ &+ \frac{1}{2} C_{jklm}(\mathbf{x}) \left( \int_{\partial V^I} \frac{\partial G_{ij}^{Im}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} + \int_{\partial V^I} \frac{\partial G_{mj}^{Im}}{\partial x_i}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right) \end{aligned} \quad (12)$$

The second term is zero for a homogenous material as it is only related to the imaginary parts of the Green tensor. Hence, the first term corresponds indeed to the expression of the Eshelby tensor for a spherical inclusion in an anisotropic homogeneous medium as can be found in (Lazar, 2016).

### 2.2.2. Uniform eigenstrain within a spherical inclusion spanning the two materials

If the inclusion spans the two materials, i.e. the center of the spherical inclusion is such that  $y_3 - R \leq 0$  and  $y_3 + R \geq 0$ , the elasticity tensor cannot be taken out of the integral. However, one can write  $\mathbf{C}(\mathbf{y}) = \mathbf{C}^{(2)} + (\mathbf{C}^{(1)} - \mathbf{C}^{(2)}) H(y_3)$  where  $H(y_3)$  is the Heaviside step function. For  $x_3 < 0$ , the following equation is thus obtained for the stress field inside the inclusion

$$\begin{aligned} \sigma_{pq}(\mathbf{x}) &= C_{pqim}^{(2)} \varepsilon_{ln}^* C_{jklm}^{(2)} \int_{V^I} \frac{\partial G_{ij}^{Bi}}{\partial y_k \partial x_m}(\mathbf{x}, \mathbf{y}) d\mathbf{y} \\ &+ C_{pqim}^{(2)} \varepsilon_{ln}^* \left( C_{jklm}^{(1)} - C_{jklm}^{(2)} \right) \int_{V^{I(1)}} \frac{\partial G_{ij}^{Bi}}{\partial y_k \partial x_m}(\mathbf{x}, \mathbf{y}) d\mathbf{y} - C_{pqim}^{(2)} \varepsilon_{im}^* \end{aligned} \quad (13)$$

where  $V^{I(1)}$  is the volume of the inclusion located in material (1). Using Eq. 8 and Gauss's theorem, we have then

$$\begin{aligned}
\sigma_{pq}(\mathbf{x}) &= C_{pqim}^{(2)} C_{jklm}^{(2)} \varepsilon_{ln}^* \left( E_{ijkm}^{(2)} + \int_{\partial V^I} \frac{\partial G_{ij}^{Im}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right) \\
&+ C_{pqim}^{(2)} \left( C_{jklm}^{(1)} - C_{jklm}^{(2)} \right) \varepsilon_{ln}^* \int_{\partial V^{I(1)}} \frac{\partial G_{ij}^{Bi}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} - C_{pqim}^{(2)} \varepsilon_{im}^*
\end{aligned} \tag{14}$$

It must be underlined that the surface area  $\partial V^{I(1)}$  represents the part of  $\partial V^I$  that belongs to material (1) plus the intersection disk between the spherical inclusion and the plane  $y_3 = 0$ . In this case, the Eshelby tensor for a spherical inclusion in a bi-material,  $\mathbf{S}^{Esh, Bi}$ , reads

$$\begin{aligned}
S_{imln}^{Esh, Bi} &= \frac{1}{2} C_{jklm}^{(2)} \left( E_{ijkm}^{(2)} + E_{mjki}^{(2)} \right) \\
&+ \frac{1}{2} C_{jklm}^{(2)} \left( \int_{\partial V^I} \frac{\partial G_{ij}^{Im}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} + \int_{\partial V^I} \frac{\partial G_{mj}^{Im}}{\partial x_i}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right) \\
&+ \frac{1}{2} \left( C_{jklm}^{(1)} - C_{jklm}^{(2)} \right) \left( \int_{\partial V^{I(1)}} \frac{\partial G_{ij}^{Bi}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} + \int_{\partial V^{I(1)}} \frac{\partial G_{mj}^{Bi}}{\partial x_i}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right)
\end{aligned} \tag{15}$$

For  $x_3 > 0$ , the same procedure leads to

$$\begin{aligned}
\sigma_{pq}(\mathbf{x}) &= C_{pqim}^{(1)} C_{jklm}^{(1)} \varepsilon_{ln}^* \left( E_{ijkm}^{(1)} + \int_{\partial V^I} \frac{\partial G_{ij}^{Im}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right) \\
&+ C_{pqim}^{(1)} \left( C_{jklm}^{(2)} - C_{jklm}^{(1)} \right) \varepsilon_{ln}^* \int_{\partial V^{I(2)}} \frac{\partial G_{ij}^{Bi}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} - C_{pqim}^{(1)} \varepsilon_{im}^*
\end{aligned} \tag{16}$$

$$\begin{aligned}
S_{imln}^{Esh, Bi} &= \frac{1}{2} C_{jklm}^{(1)} \left( E_{ijkm}^{(1)} + E_{mjki}^{(1)} \right) \\
&+ \frac{1}{2} C_{jklm}^{(1)} \left( \int_{\partial V^I} \frac{\partial G_{ij}^{Im}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} + \int_{\partial V^I} \frac{\partial G_{mj}^{Im}}{\partial x_i}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right) \\
&+ \frac{1}{2} \left( C_{jklm}^{(2)} - C_{jklm}^{(1)} \right) \left( \int_{\partial V^{I(2)}} \frac{\partial G_{ij}^{Bi}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} + \int_{\partial V^{I(2)}} \frac{\partial G_{mj}^{Bi}}{\partial x_i}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right)
\end{aligned} \tag{17}$$

### 2.2.3. Cubic elastic and dilatational eigenstrain

In the case of cubic elasticity and for a dilatational eigenstrain of the form

$$\boldsymbol{\varepsilon}^* = \begin{bmatrix} \delta^* & 0 & 0 \\ 0 & \delta^* & 0 \\ 0 & 0 & \delta^* \end{bmatrix} \quad (18)$$

it is noteworthy that  $(C_{ijkln}^{(2)} - C_{ijkln}^{(1)})\varepsilon_{ln}^* = 0 \forall j, \forall k$ . Hence, Eqs. 14 and 16 reduce seemingly to Eq. 11, namely, for  $x_3 < 0$

$$\sigma_{pq}(\mathbf{x}) = C_{pqim}^{(2)} \left( C_{ijkln}^{(2)} \varepsilon_{ln}^* \left( E_{ijkm}^{(2)} + \int_{\partial V^I} \frac{\partial G_{ij}^{Im}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right) - \varepsilon_{im}^* \right) \quad (19)$$

and for  $x_3 > 0$

$$\sigma_{pq}(\mathbf{x}) = C_{pqim}^{(1)} \left( C_{ijkln}^{(1)} \varepsilon_{ln}^* \left( E_{ijkm}^{(1)} + \int_{\partial V^I} \frac{\partial G_{ij}^{Im}}{\partial x_m}(\mathbf{x}, \mathbf{y}) n_k d\mathbf{y} \right) - \varepsilon_{im}^* \right) \quad (20)$$

However, at the difference of Eq. 11, the computation of  $\mathbf{G}^{Im}$  involves the use of full-space terms (see Eqs. B.14 and B.20) when the inclusion spans the two materials, which has consequences on the numerical integration speed (see further Section 3.1). Finally, it can be noticed that the stress components  $\sigma_{pq}$  scale directly with  $\delta^*$  in this case.

### 2.3. Elastic strain energy

The elastic strain energy is defined as

$$W^e = \frac{1}{2} \int_V \sigma_{ij}(\mathbf{x}) \varepsilon_{ij}^e(\mathbf{x}) d\mathbf{x} \quad (21)$$

where  $\boldsymbol{\varepsilon}^e$  is the elastic strain tensor. When eigenstrains are prescribed in  $V^I$  and in the absence of any external force and surface constraint,  $W^e$  writes (Mura, 1987; Berbenni et al., 2008)

$$W^e = -\frac{1}{2} \int_{V^I} \sigma_{ij}(\mathbf{x}) \varepsilon_{ij}^*(\mathbf{x}) d\mathbf{x} \quad (22)$$

For a uniform dilatational eigenstrain of the form of Eq. 18 ( $\varepsilon_{ij}^* = \delta^* \delta_{ij}$ ),  $W^e$  scales thus with  $\delta^{*2}$  since  $\sigma_{ij}$  scales also with  $\delta^*$  (see Eqs. 19-20).

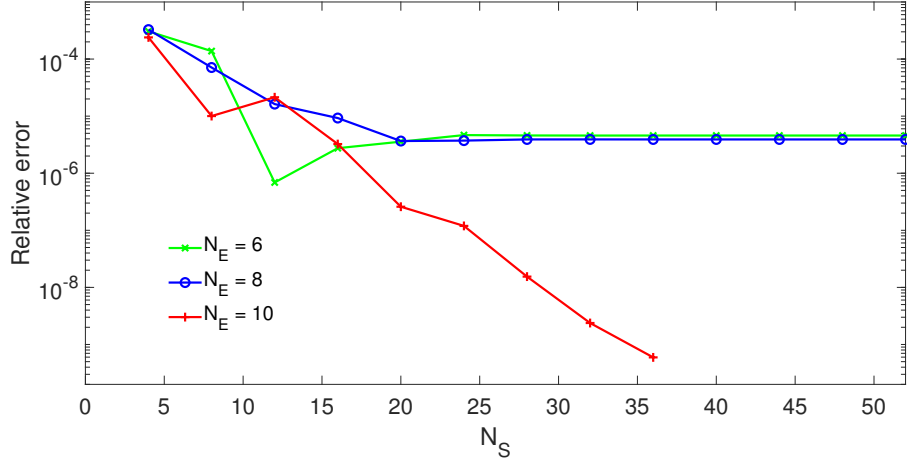


Figure 2: Relative error made on the computation of the elastic strain energy (Eq. 22) as a function of  $N_S$  for different values of  $N_E$  for an inclusion centered at  $y_3 = -1.1R$ . The reference value is considered at  $N_S = 52$  and  $N_E = 10$ .

### 3. Numerical implementation

The numerical integrations over  $[0, \pi]$  involved in the calculation of  $E_{ijklm}$  and  $\frac{\partial G_{ij}^{Im}}{\partial x_m}$  are performed with the function *integral* of the software *MATLAB R2022a*. They are used in conjunction with the *eig* function to solve the Stroh eigenrelation (Eq. B.7). The numerical integrations over  $\partial V^I$ ,  $\partial V^{I(1)}$ ,  $\partial V^{I(2)}$  and  $V^I$  are obtained from a Gauss quadrature method. The order of the Legendre polynomials are denoted  $N_S$  for integrals over surfaces to compute the stresses ( $N_S \times N_S$  integration points) and  $N_E$  for integrals over volumes to get the elastic strain energy ( $N_E \times N_E \times N_E$  integration points).

#### 3.1. Convergence study

For the convergence study, a uniform dilatational eigenstrain of the form of Eq. 18 with  $\delta^* = 0.1$  is considered along with cubic elastic constants of Cu,  $C_{11} = 170$  GPa,  $C_{12} = 124$  GPa,  $C_{44} = 75$  GPa, a spherical inclusion's radius  $R = \frac{a_0\sqrt{2}}{4}$  with the lattice parameter  $a_0 = 0.36149$  nm and crystallographic orientations corresponding to 'Orientation A' in Table 1.

Figure 2 shows the relative error made on the computation of the elastic strain energy (Eq. 22) as a function of  $N_S$  for an inclusion centered at

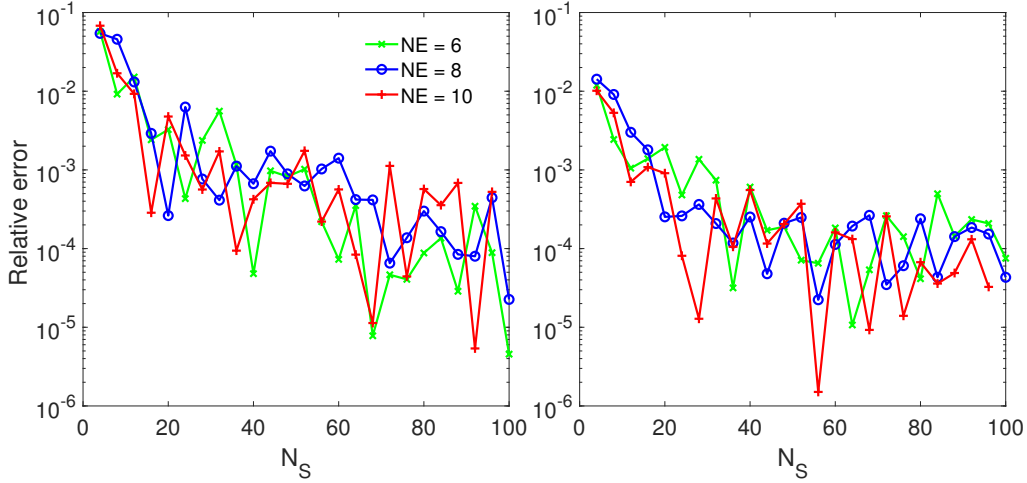


Figure 3: Relative error made on the computation of the elastic strain energy (Eq. 22) as a function of  $N_S$  for different values of  $N_E$  for an inclusion centered at  $y_3 = -0.5R$  (left) and at  $y_3 = 0$  (right). The reference values are considered at  $N_S = 100$  and  $N_E = 10$ .

$y_3 = -1.1R$  and values of  $N_E$  ranging from 6 to 10. In this case, the computations of the stresses involves Eq. 11 since the inclusion completely belongs to material (2). It is seen then that a rapid convergence is obtained. A very high accuracy is achieved for  $N_S > 20$  with relative errors less than  $5 * 10^{-6}$ .

Figure 3 shows then the relative error made on the computation of the elastic strain energy (Eq. 22) for an inclusion centered at  $y_3 = -0.5R$  and at  $y_3 = 0$ . In this case, the computations of the stresses involves Eqs. 19 and 20 since the inclusion spans to the two materials. Numerically, the main difference with Eq. 11 lies in the computation of  $\mathbf{G}^{Im}$  which involves the use of full-space terms (see Eqs. B.14 and B.20) only when the inclusion spans the two materials. Hence, surface integrals of first derivative of full-space Green tensors must be computed over the part of  $\partial V^I$  that belongs to material (1) or (2) and this increases considerably the time needed to achieve an acceptable numerical precision. The convergence is thus much more difficult. However, for  $N_S > 60$ , the relative error remains below  $10^{-3}$  which is acceptable. In both Figures 2 and 3, it can be observed that increasing the value of  $N_E$  above 6 has only a marginal effect. Therefore, it is pointless to increase  $N_E$  if the stresses within the inclusion are not evaluated with enough accuracy.

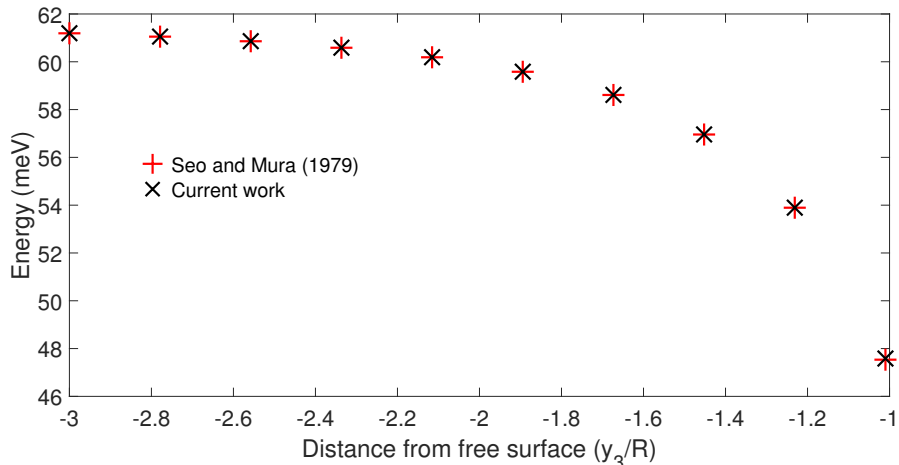


Figure 4: Comparison of energy variation towards a free surface for a spherical inclusion with a uniform dilatational eigenstrain  $\varepsilon_{ij}^* = 0.1\delta_{ij}$ . The solution of Seo and Mura (1979) is computed from Eq. 23 whereas the solution corresponding to the current work is obtained from Eqs. 22, 19, 24 and 25.  $\mu = 23$  GPa,  $\nu = 0.4218$  and  $R = 0.1278$  nm.

### 3.2. Comparison with the known solution in an isotropic half-space

Seo and Mura (1979) have solved the problem of an ellipsoidal inclusion with a uniform dilatational eigenstrain of the form of Eq. 18 located in an isotropic half-space (see also (Mura, 1987)). With our notations, the elastic strain energy for a sphere reads in this case

$$W^e = 2\mu \frac{1+\nu}{1-\nu} \delta^{*2} V^I \left( 1 - \frac{1+\nu}{6} \left( \frac{R}{y_3} \right)^3 \right) \quad (23)$$

where  $\nu$  is the Poisson coefficient and  $\mu$  the shear modulus.  $y_3$  stands for the position of the inclusion center and  $y_3 = 0$  corresponds to the free surface. This analytical solution can serve as a reference to check the correctness of the numerical implementation performed in this work. However, in isotropic media, the Stroh eigenvalues which are solutions of Eq. B.7 are not distinct (Bacon et al., 1980). This problem can be circumvented by considering the Stroh integral formalism (Bacon et al., 1980) in which such degeneracies never appear. An alternative approximate approach, that is nevertheless quite satisfactory from the numerical point of view, is to compute  $C_{44}$  as

$$C_{44} = 1.0001 \frac{C_{11} - C_{12}}{2} \quad (24)$$

In the same way, anisotropic Green’s function for half-space do exist (Barnett and Lothe, 1975; Pan and Yuan, 2000). However, for the present purpose of checking the equations implementation, it was chosen to simply set

$$\mathbf{C}^{(2)} = 10^{-10} \mathbf{C}^{(1)} \quad (25)$$

Hence, the comparison was made using Eqs. 22, 19, 24 and 25 on one side and Eq. 23 with  $\mu = (C_{11} - C_{12})/2$  and  $\nu = C_{12}/(2(C_{12} + \mu))$  on the other side. The same values as for the convergence study (Section 3.1) were considered for  $C_{11}$ ,  $C_{12}$ ,  $\delta^*$  and  $R$ . Figure 4 displays the elastic strain energy variation with the distance to the free surface for the two solutions. A perfect numerical match is obtained. It is noteworthy that the energy variation scales as  $\left(\frac{R}{y_3}\right)^3$  and that the energy always decreases when approaching the free surface meaning that the free surface attracts the inclusion.

## 4. Results

### 4.1. Interior stress fields

#### 4.1.1. Dilatational eigenstrain

Considering the same parameters as for the convergence study (Section 3.1), i.e. a spherical inclusion with a uniform dilatational eigenstrain of the form of Eq. 18 with  $\delta^* = 0.1$ , cubic elastic constants of Cu and ‘Orientation A’ of Table 1, the stresses within the inclusion for different positions of the inclusion with respect to the interface were computed using Eqs. 19 and 20. The order of the Legendre polynomials was set to  $N_S = 30$  when the inclusion belongs to a same material and to  $N_S = 100$  when the inclusion spans the two materials. Figures 5, 6, 7 and 8 show the variations along  $\mathbf{e}_3$  of the stress components which are not negligible for the particular crystallographic orientations considered. ‘Orientation A’ is supposed to provide strong contrast between the two materials since the directions [111] and [001], respectively the strongest and the weakest direction for the directional Young modulus (Richeton, 2019), are facing each other along  $\mathbf{e}_3$ .

The first observation is that the stresses are not uniform within the inclusion at the difference of the well-known Eshelby’s result of uniform stresses

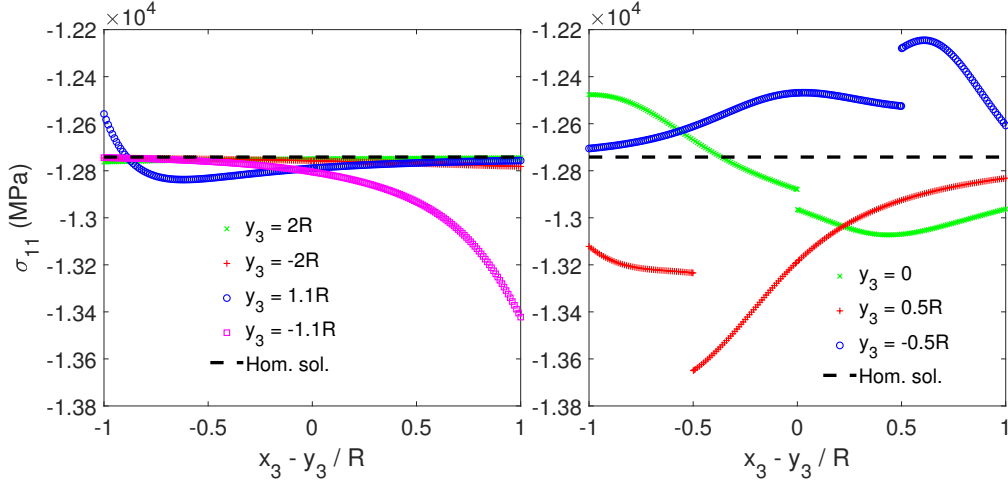


Figure 5: Variation of  $\sigma_{11}$  along  $\mathbf{e}_3$  ( $x_1 = x_2 = 0$ ) for a dilatational eigenstrain  $\varepsilon_{ij}^* = 0.1\delta_{ij}$ . Different positions ( $y_1 = y_2 = 0, y_3$ ) of the inclusion center are considered on both sides of the interface. The dashed line represents the solution in the homogeneous medium.

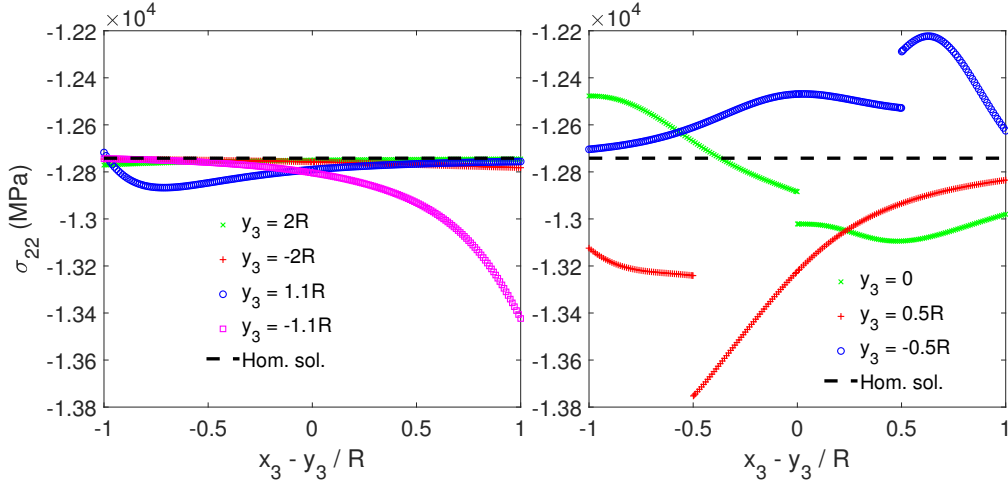


Figure 6: Variation of  $\sigma_{22}$  along  $\mathbf{e}_3$  ( $x_1 = x_2 = 0$ ) for a dilatational eigenstrain  $\varepsilon_{ij}^* = 0.1\delta_{ij}$ . Different positions ( $y_1 = y_2 = 0, y_3$ ) of the inclusion center are considered on both sides of the interface. The dashed line represents the solution in the homogeneous medium.

for ellipsoidal inclusions with uniform eigenstrain in homogeneous media (Eshelby, 1957). Besides, it is noteworthy that for a dilatational eigenstrain, due to the cubic symmetry, we have  $(E_{jkl n}^{(2)} - E_{jkl n}^{(1)}) \varepsilon_{ln}^* = 0 \forall j, \forall k$ , in addition to



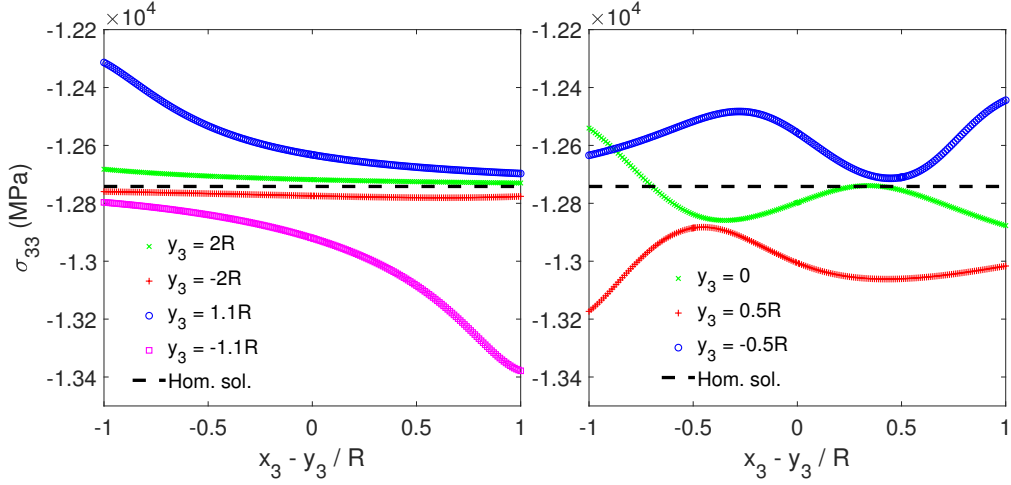


Figure 7: Variation of  $\sigma_{33}$  along  $\mathbf{e}_3$  ( $x_1 = x_2 = 0$ ) for a dilatational eigenstrain  $\varepsilon_{ij}^* = 0.1\delta_{ij}$ . Different positions ( $y_1 = y_2 = 0, y_3$ ) of the inclusion center are considered on both sides of the interface. The dashed line represents the solution in the homogeneous medium.

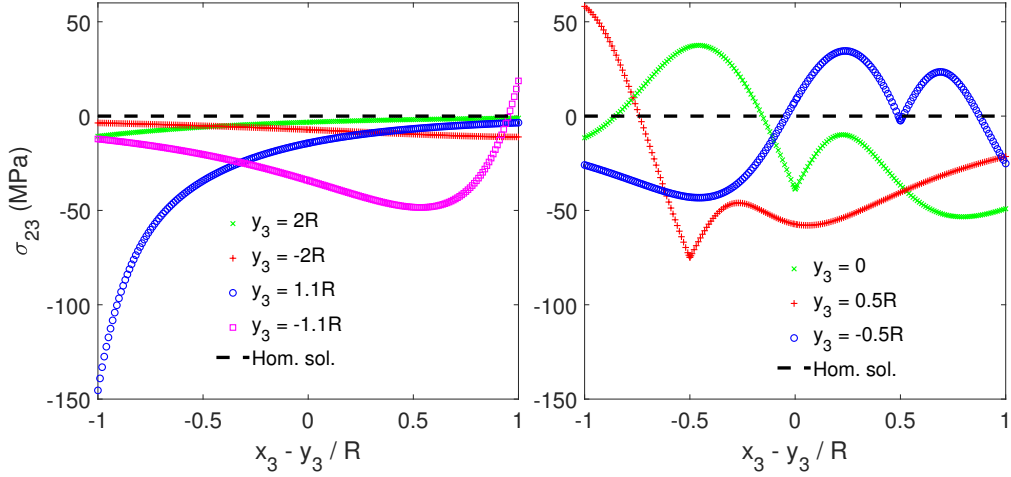


Figure 8: Variation of  $\sigma_{23}$  along  $\mathbf{e}_3$  ( $x_1 = x_2 = 0$ ) for a dilatational eigenstrain  $\varepsilon_{ij}^* = 0.1\delta_{ij}$ . Different positions ( $y_1 = y_2 = 0, y_3$ ) of the inclusion center are considered on both sides of the interface. The dashed line represents the solution in the homogeneous medium.

$(C_{jklm}^{(2)} - C_{jklm}^{(1)}) \varepsilon_{ln}^* = 0 \forall j, \forall k$  (see Section 2.2.3). Hence, the stress solutions in a homogeneous medium (see Eqs. 19 or 20 with  $\mathbf{G}^{Im} = 0$ ) do not depend on the crystallographic orientation. They are the same considering material (2)

or material (1) as the reference homogenous medium. Therefore the stress variations cannot be interpreted as smooth transitions from given values in material (2) to different values in material (1). The effect of the imaginary term  $\mathbf{G}^{Im}$  is much more complex. It is also important to underline that the stress variations are homothetic with respect to the inclusion radius  $R$ .

As it can be expected, when the inclusion belongs to an unique material, the further away from the interface, the more important is the deviation from the homogeneous reference solution. This deviation is asymmetric as it is much more pronounced on the side of the interface. Nevertheless, it should be noticed that the stress variations are not necessarily monotonous, see e.g.,  $\sigma_{11}$  and  $\sigma_{22}$  at  $y_3 = 1.1R$  and  $\sigma_{23}$  at  $y_3 = -1.1R$ . The stress variations can be significant close to the interface (i.e., for  $y_3 = \pm 1.1R$ ) with stress differences greater than 600 MPa and relative variations greater than 5%. However, it seems that these stress differences rapidly decrease as one moves away from the interface as can be noticed from the relative small departures of the Eshelby's homogeneous solutions at  $y_3 = \pm 2R$ .

When the inclusion spans the two materials, it can be checked that the tractions continuity is well respected (see  $\sigma_{33}$  and  $\sigma_{23}$ ). It can be also observed that the stress jumps for  $\sigma_{11}$  and  $\sigma_{22}$  are more important at  $y_3 = \pm 0.5R$  than at  $y_3 = 0$ . There is also clear departures from the reference homogeneous stress solutions, even at  $y_3 = 0$ , showing that there is no compensation of the imaginary term contributions. Stress variations are never monotonous and are much more disturbed than when the inclusion belongs to a same material. Stress differences within the inclusion can also be very high, e.g., approaching 1 GPa for  $\sigma_{22}$  at  $y_3 = 0.5R$ .

For illustration purposes, variations of stresses along  $\mathbf{e}_1$  through the center of the spherical inclusion are also shown in Figures 9 and 10 at  $y_3 = \pm 2R$  and  $y_3 = \pm 1.1R$ . In this case too, the stresses are non homogeneous although the distance from the interface does not change. For the particular ‘Orientation A’ considered, the stress variations are either symmetric for  $\sigma_{11}$ ,  $\sigma_{22}$ ,  $\sigma_{33}$  and  $\sigma_{23}$  or anti-symmetric for  $\sigma_{31}$  and  $\sigma_{12}$ . As expected, the variations are much more pronounced at  $y_3 = \pm 1.1R$  than at  $y_3 = \pm 2R$ . They are also globally weaker than along  $\mathbf{e}_3$ , which makes sense since the distance from the interface is fixed.

#### 4.1.2. Shear eigenstrain

Still considering the cubic elastic constants of Cu and ‘Orientation A’ of Table 1, a spherical inclusion with a uniform shear eigenstrain of the form of

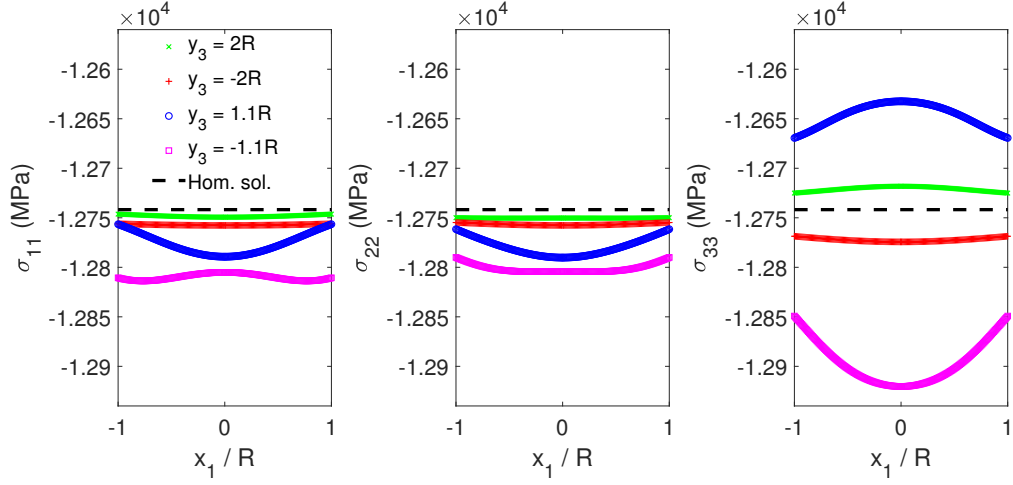


Figure 9: Variation of  $\sigma_{11}$ ,  $\sigma_{22}$  and  $\sigma_{33}$  along  $e_1$  ( $x_2 = 0$ ,  $x_3 = y_3$ ) for a dilatational eigenstrain  $\varepsilon_{ij}^* = 0.1\delta_{ij}$ . Different positions ( $y_1 = y_2 = 0, y_3$ ) of the inclusion center are considered on both sides of the interface. The dashed line represents the solution in the homogeneous medium.

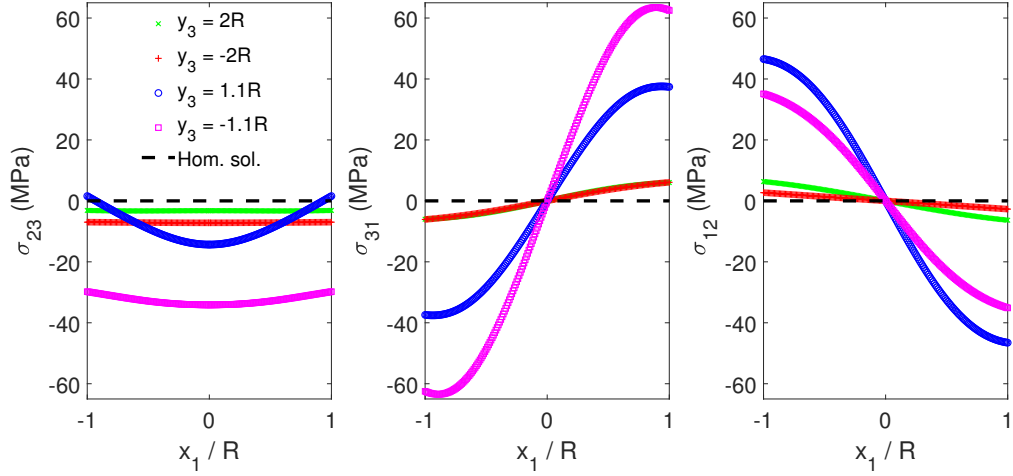


Figure 10: Variation of  $\sigma_{23}$ ,  $\sigma_{31}$  and  $\sigma_{12}$  along  $e_1$  ( $x_2 = 0$ ,  $x_3 = y_3$ ) for a dilatational eigenstrain (Eq. 18 with  $\delta = 0.1$ ). Different positions ( $y_1 = y_2 = 0, y_3$ ) of the inclusion center are considered on both sides of the interface. The dashed line represents the solution in the homogeneous medium (i.e.,  $y_3 = \infty$ ).

Eq. 26 below is now assumed.

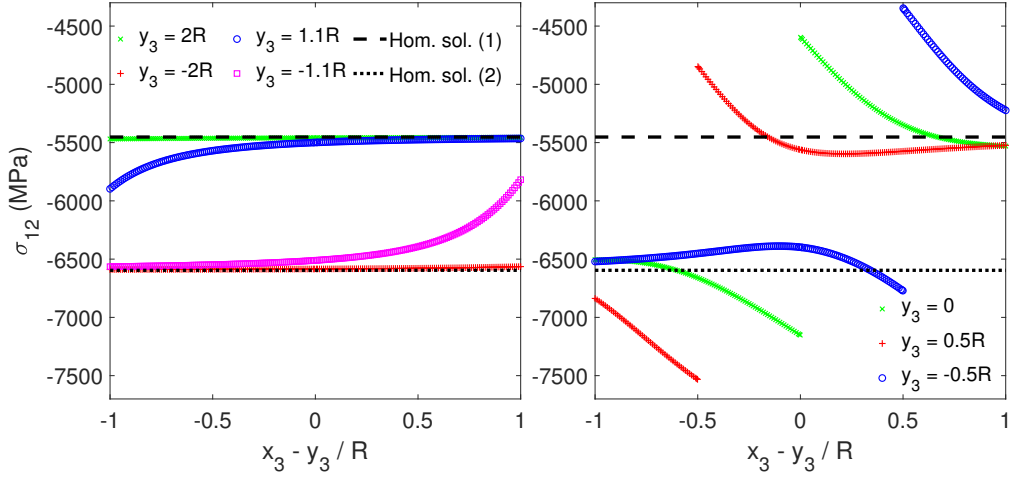


Figure 11: Variation of  $\sigma_{12}$  along  $\mathbf{e}_3$  ( $x_1 = x_2 = 0$ ) for a shear eigenstrain (Eq. 26). Different positions ( $y_1 = y_2 = 0, y_3$ ) of the inclusion center are considered on both sides of the interface. The dashed and dotted lines represent the solutions in the homogeneous media.

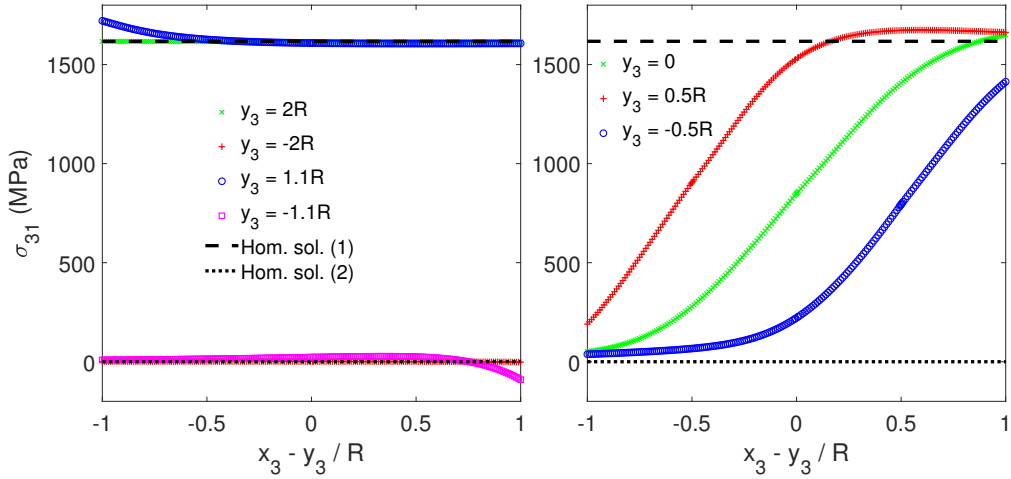


Figure 12: Variation of  $\sigma_{31}$  along  $\mathbf{e}_3$  ( $x_1 = x_2 = 0$ ) for a shear eigenstrain (Eq. 26). Different positions ( $y_1 = y_2 = 0, y_3$ ) of the inclusion center are considered on both sides of the interface. The dashed and dotted lines represent the solutions in the homogeneous media.

$$\varepsilon^* = \begin{bmatrix} 0 & 0.1 & 0 \\ 0.1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad (26)$$

It is noteworthy that, in this case, the homogenous reference solutions are different between materials (1) and (2). Figures 11 and 12 show the variations along  $\mathbf{e}_3$  of  $\sigma_{12}$  and  $\sigma_{31}$  (i.e., the two components which are not negligible for the particular crystallographic orientations considered). Same general remarks as for the dilatational eigenstrain hold: non-homogeneous stresses and not necessarily monotonous variations are observed, as well as a rapid decrease of the departure from the homogeneous solution when one moves away from the interface. When the inclusion spans the two materials, the continuity of  $\sigma_{31}$  is well respected while the stress jumps displayed by  $\sigma_{12}$  are very high with a jump greater than 2.5 GPa at  $y_3 = 0.5R$ .  $\sigma_{31}$  exhibits very strong stress gradients which seem to be controlled by the difference between the homogenous reference solutions of materials (1) and (2).

#### 4.2. Variation of elastic strain energy

The variation of the elastic strain energy (Eq. 22) with respect to the position of the inclusion center from one side to the other side of the interface are computed for the different crystallographic orientations considered in Table 1 and different uniform eigenstrains (dilatational (Eq. 18) and shear (Eq. 26)).

While in ‘Orientation A’, the two extreme directions for the directional Young modulus, [111] and [001], are facing each other along  $\mathbf{e}_3$ , i.e., in a normal way to the interface, these two directions are facing each other along  $\mathbf{e}_1$ , i.e., in a parallel way to the interface, in ‘Orientation B’. ‘Orientation A’ and ‘Orientation B’ have the same misorientation angle of  $56.6^\circ$ . In ‘Orientation C’ the direction [111] is along  $\mathbf{e}_3$  in material (1) and along  $\mathbf{e}_1$  in material (2). ‘Orientation C’ yields a misorientation angle of  $42.8^\circ$ . In addition, crystallographic orientations corresponding to symmetrical pure tilt boundaries composed of an infinite array of edge dislocations are also considered (Hirth and Lothe, 1982). In the initial configuration, the Burgers vectors  $[\bar{1}11]$  is along  $\mathbf{e}_3$  while the dislocation line direction [112] is along  $\mathbf{e}_2$ . Starting from this orientation, the stiffness tensors are rotated by  $-\theta/2$  and  $\theta/2$  around  $\mathbf{e}_2$  in materials (2) and (1), respectively, where  $\theta$  is the tilt or misorientation angle (Hirth and Lothe, 1982). Two cases are computed,  $\theta = 11.5^\circ$  and  $\theta = 19.1^\circ$  which correspond approximately to  $h/b = 5$  and  $h/b = 3$ , respectively, with  $b$  the Burgers vector magnitude and  $h$  the spacing between dislocations in the periodic wall.

For these applications, the order of the Legendre polynomials was set to  $N_E = 6$  for integrals over volumes. For integral over surfaces, the order was

set to  $N_S = 20$  when the inclusion belongs to a same material. When the inclusion spans the two materials,  $N_S = 60$  was used for ‘Orientations A, B and C’ (Table 1) and  $N_S = 100$  for the two symmetrical tilt boundaries as the energy variation is much weaker in these cases and thus required a higher numerical precision.

	Material (1)	Material (2)	Misorientation angle
Orientation A	$\begin{bmatrix} 111 \\ 11\bar{2} \end{bmatrix} \parallel \mathbf{e}_3$ $\begin{bmatrix} 111 \\ 11\bar{2} \end{bmatrix} \parallel \mathbf{e}_2$	$\begin{bmatrix} 001 \\ 010 \end{bmatrix} \parallel \mathbf{e}_3$ $\begin{bmatrix} 001 \\ 010 \end{bmatrix} \parallel \mathbf{e}_2$	56.6 °
Orientation B	$\begin{bmatrix} 111 \\ 11\bar{2} \end{bmatrix} \parallel \mathbf{e}_1$ $\begin{bmatrix} 111 \\ 11\bar{2} \end{bmatrix} \parallel \mathbf{e}_2$	$\begin{bmatrix} 100 \\ 010 \end{bmatrix} \parallel \mathbf{e}_1$ $\begin{bmatrix} 100 \\ 010 \end{bmatrix} \parallel \mathbf{e}_2$	56.6 °
Orientation C	$\begin{bmatrix} 111 \\ 11\bar{2} \end{bmatrix} \parallel \mathbf{e}_3$ $\begin{bmatrix} 111 \\ 11\bar{2} \end{bmatrix} \parallel \mathbf{e}_2$	$\begin{bmatrix} 111 \\ 11\bar{2} \end{bmatrix} \parallel \mathbf{e}_1$ $\begin{bmatrix} 111 \\ 11\bar{2} \end{bmatrix} \parallel \mathbf{e}_2$	42.8 °

Table 1: Different crystallographic orientations considered for the two materials.

#### 4.2.1. Dilatational eigenstrain

For a uniform dilatational eigenstrain of the form of Eq. 18,  $W^e$  scales with  $\delta^{*2}$  as explained in Section 2.3 and for cubic elasticity, as for the stresses, the energy in a homogenous medium does not depend on the particular crystallographic orientation. Moreover, if the stress variations are homothetic with respect to the inclusion radius  $R$ , the elastic strain energy scales with the inclusion volume (cf. Eq. 22). For these reasons, Fig. 13 displays the relative energy variation for the five orientations considered with respect to the homogeneous reference energy. The quantitative aspect of the variation will be discussed later in Section 5. Since the energy should go back to the same value in each material, energy variations are necessarily non-homogeneous as shown by Fig. 13. There are however three to four local extrema depending on the orientation considered. The variations are really significant only within the range  $-1.5R < y_3 < 1.5R$ . In the range where the inclusion belongs to a single material (i.e.,  $y_3 < -R$  or  $y_3 > R$ ), it can be conjectured that the departure from the homogeneous reference energy, i.e. the decrease of the imaginary term, probably follows the same scaling of  $\left(\frac{R}{y_3}\right)^3$  (cf. Eq. 23) as the imaginary term in an isotropic half-space (Seo and Mura, 1979; Mura, 1987).

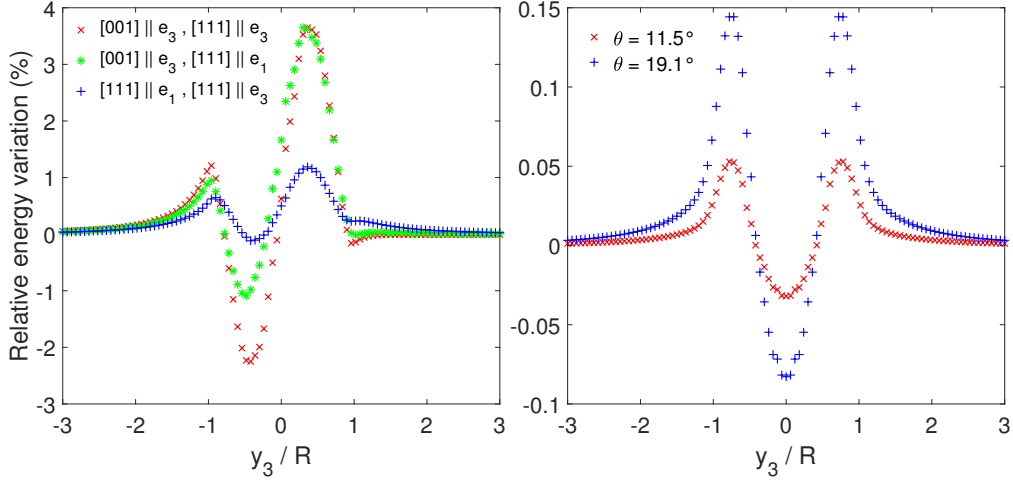


Figure 13: Relative energy variation with respect to the homogeneous reference energy for a dilatational eigenstrain (Eq. 18) when the position of the inclusion center ( $y_3$ ) is displaced from one side to the other side of the interface along  $\mathbf{e}_3$ . On the left, comparison between the three orientations of Table 1. On the right, comparison between the two symmetrical tilt boundaries ( $\theta$  being the tilt angle).

For the symmetrical tilt boundaries, the variations are perfectly symmetric with a global minimum at  $y_3 = 0$  that decreases with the tilt angle. For the orientations of Table 1, a rapid transition is observed, around  $y_3 = 0$ , from the global minimum on one side of the interface to the global maximum on the other side of the interface. It is noteworthy that the global minimum and maximum always correspond to configurations where the inclusion spans the two materials. ‘Orientations A’ exhibits the lowest minimum, followed by ‘Orientations B’ and ‘Orientations C’, which agrees with the supposed elastic contrast for a dilatation displayed by these orientations.

#### 4.2.2. Shear eigenstrain

For the shear eigenstrain of Eq. 26, the energy in a homogenous medium depends on the particular crystallographic orientation. It is however identical in materials (1) and (2) when the latter refer to the orientations on both side of a symmetrical tilt boundary. Therefore, for ‘Orientations A, B and C’, the energy variation does not go through an extremum value. There is a smooth transition from from the reference homogeneous energy in one material to the reference homogeneous energy in the other material over the range  $-1.5R < y_3 < 1.5R$ . For the symmetrical tilt boundaries, the energy

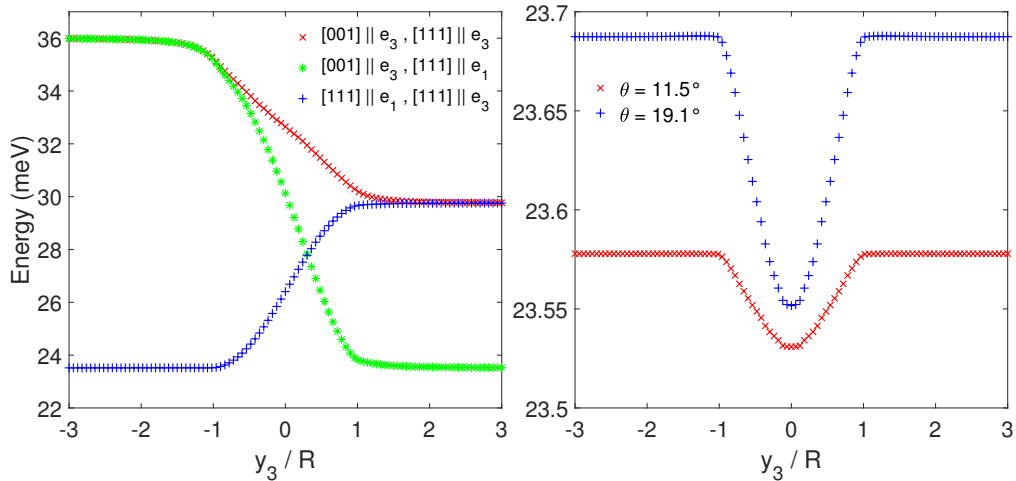


Figure 14: Energy variation for the shear eigenstrain of Eq. 26 when the position of the inclusion center ( $y_3$ ) is displaced from one side to the other side of the interface along  $\mathbf{e}_3$ . On the left, comparison between the three orientations of Table 1. On the right, comparison between the two symmetrical tilt boundaries ( $\theta$  being the tilt angle).

variations are perfectly symmetric and go through a single minimum at  $y_3 = 0$  that decreases with the tilt angle.

## 5. Discussion

The dilatational eigenstrain tensor considered in Eq. 18 is well-suited for modeling the effects of vacancies or solute atoms in substitution in cubic lattices (White and Coghlan, 1977; Cai et al., 2014; Dingreville and Berbenni, 2016; Clouet et al., 2018). However, examining the segregation of such defects toward grain boundaries requires considering various other important factors. First, the interaction with the stress field resulting from the grain boundary should be taken into account as well. Two primary contributions are typically associated with this interaction (White and Coghlan, 1977; Clouet et al., 2018): a size effect linked to the dilatation considered in the eigenstrain and a modulus effect stemming from the fact that the presence of solutes alters the elastic constants of the material. Secondly, grain boundaries possess small, albeit finite, width (of the order of the nanometer), unlike the singular interface examined in this study. Therefore, it is certainly worthwhile to consider a specific elastic stiffness tensor over the grain boundary width, as done in previous studies (Chen et al., 2019, 2020, 2021). For the symmetrical



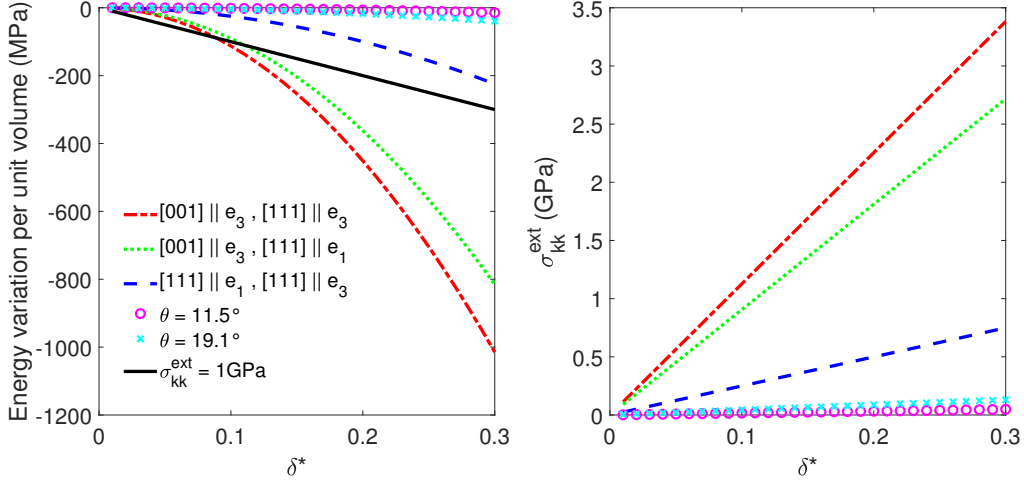


Figure 15: On the left, maximum energy variation due to image effect with respect to  $\delta^*$  considering a dilatational eigenstrain  $\varepsilon_{ij}^* = \delta^* \delta_{ij}$  and the three orientations of Table 1, as well as the two symmetrical tilt boundaries defined by their tilt angle  $\theta$ . These variations are compared to the interaction energy (cf. Eq.28) between the same eigenstrain and an external stress field defined by the value of its trace,  $\sigma_{kk}^{ext} = 1 \text{ GPa}$ . On the right is plotted the equivalent value of  $\sigma_{kk}^{ext}$  such that the maximum energy variation due to the image effect equals the interaction energy between the dilatational eigenstrain and  $\sigma_{kk}^{ext}$ .

tilt boundaries, a smooth transition from  $\mathbf{C}^{(2)}$  to  $\mathbf{C}^{(1)}$  is nevertheless rather expected at the scale of a few nanometers. Additionally, elasticity may be nonlinear within certain regions of the grain boundary. Thus, the configuration where the inclusion spans the two materials does reflect a direct reality but it might provide insights into the impact of elastic heterogeneity when the defect is within the grain boundary, especially as the defect size becomes comparable to the grain boundary size, as with large precipitates.

However, it might be valuable to quantitatively compare the image effect felt by a dilatation center in heterogeneous anisotropic elasticity (Fig. 13) to the typical size effect associated with the interaction energy between a dilatation center and a grain boundary stress field. The latter can be determined from the general elastic interaction energy between an eigenstrain  $\varepsilon^*$  distributed in  $V^I$  and an external stress field  $\sigma^{ext}$  (such as the one arising from a grain boundary), as given by (Mura, 1987)

$$W^{int} = - \int_{V^I} \sigma_{ij}^{ext}(\mathbf{x}) \varepsilon_{ij}^*(\mathbf{x}) d\mathbf{x} \quad (27)$$

Considering that the volume  $V^I$  is sufficiently small to disregard variations of the external stress field within it, we can write for a uniform dilatational eigenstrain of the form  $\varepsilon_{ij}^* = \delta^* \delta_{ij}$

$$W^{int} = -V^I \delta^* \sigma_{kk}^{ext} \quad (28)$$

Figure 15 displays on the left the maximum energy variation per unit volume due to the image effect with respect to  $\delta^*$  considering the three orientations of Table 1 and the two symmetrical tilt boundaries. These variations are directly inferred from Fig. 13. They are then compared to the interaction energy per unit volume computed from Eq. 28 between the same dilatational eigenstrain and an external stress field with a trace value of 1 GPa. As anticipated, the image effect scales with  $\delta^{*2}$ , while the interaction energy with a stress field scales linearly with  $\delta^*$ . In the current scenario with  $\sigma_{kk}^{ext} = 1$  GPa, the image effect becomes predominant for ‘Orientations A and B’ when  $\delta^* > 0.1$ . To quantitatively evaluate the significance of the image effect, Figure 15 then presents, on the right, the equivalent value of  $\sigma_{kk}^{ext}$  such that the maximum energy variation due to the image effect equals the interaction energy between the dilatational eigenstrain and  $\sigma_{kk}^{ext}$  according to Eq. 28. These  $\sigma_{kk}^{ext}$  values scale therefore linearly with  $\delta^*$ . While these values remain very low for the symmetrical tilt boundaries, they can be comparable to typical values of grain boundary stress fields (Dingreville and Berbenni, 2016) for the other orientations considered (cf. Table 1). Furthermore, Figure 15 emphasizes that the larger the dilatation of the inclusion, the more likely the image effect is to be significant compared to the interaction energy with a stress field (Eq. 28) due to the different scaling. Another distinction should be pointed out. The image effect remains indeed the same at a given distance from the interface. On the contrary, the interaction energy varies with the grain boundary stress field (Eq. 28), thus exhibiting strong variations along the grain boundary that range from negative to positive values (White and Coghlan, 1977; Dingreville and Berbenni, 2016).

In addition to the dilatation value, several other factors influence the significance of the image effect, such as the degree of elastic anisotropy and the extent of elastic heterogeneity. Elastic heterogeneity can be associated with misorientations between grains but also to the presence of different phases (heterophase interfaces) or to materials of different kinds as in composites. The present results were obtained for Cu, which has a relatively high Zener ratio with  $A = \frac{2C_{44}}{C_{11} - C_{12}} = 3.26$ . However, certain cubic materials can ex-

hibit much higher values of  $A$ , like lithium metal with  $A \approx 8$  (Aspinall et al., 2022), a crucial component in batteries, or some shape memory alloys like CuAlBe with  $A \approx 13$  (Rios-Jara et al., 1991). Nevertheless, the image effect is expected to increase asymptotically with  $A$  since the maximum image effect should occur in presence of free or rigid surfaces as it was computed for dislocations (Chen et al., 2021).

The exploration of non-cubic elasticity could be intriguing also. First, in a homogeneous medium, the energy due to a dilatational eigenstrain will depend on the specific crystallographic orientation. Second, the dilatational eigenstrain tensor used to simulate the role of point defects as dilatation centers should not be considered isotropic, as in Eq. 18, but should be anisotropic with the same or lower symmetry as the host lattice (Nye, 1957; Balluffi, 2016). In other words, the solute atoms should be viewed as anisotropic centers of dilatation (Cochardt et al., 1955; Siems, 1968; Clouet et al., 2018).

Finally, it may be worth underlying that the image effect might impact interface motion. Indeed, when an interface, such as a grain boundary, starts moving in presence of a distribution of defects (solutes, precipitates or vacancies), the elastic strain energy will be altered because it depends on the relative distance of the defects to the interface in heterogeneous elasticity. Hence, the elastic strain energy can increase or decrease and thus can either promote or hinder interface motion. The significance of such an image effect on interface motion was previously studied for distributions of dislocations (Richeton et al., 2020), providing insights into the connection between interface motion and crystallographic disorientations.

## 6. Conclusions

In this work, expressions of the interior stress fields of a spherical inclusion with a uniform eigenstrain embedded in an anisotropic bi-material are derived. They involve surface integrals of the imaginary term of the first derivative of the Green tensor in an anisotropic bi-material with a planar interface. The latter can be computed via the Stroh formalism from a regular line-integral over  $[0, \pi]$  as proposed by Pan and Yuan (2000). The entire expression is thus amenable to standard numerical integrations such as Gauss quadrature methods. Specific expressions are provided based on whether the inclusion belongs to the same or the two materials. Additionally, expressions for the equivalent Eshelby tensor are presented. It is noteworthy that straightforward derivations from Eq. 5 allow for expressions of both exter-

nal and internal stress fields for inclusions of any shape with non-uniform eigenstrain in anisotropic bi-materials. However, the exploration of efficient numerical integration methods for these cases remains an avenue for future investigation.

The stress fields within the spherical inclusion, along with the elastic strain energy, are then computed, taking into account the cubic elastic constants of Cu. Various inclusion positions relative to the interface, different forms of eigenstrain (dilatational (Eq.18) and pure shear (Eq.26)), and different crystallographic orientations are considered. The following key conclusions emerge:

- In a bi-material, the stresses within the inclusion are non-homogeneous, and their variations are not necessarily monotonous even when the inclusion belongs to a same material. A rapid decrease in the imaginary term is observed as one moves away from the interface.
- With a dilatational eigenstrain, the variation of elastic strain energy can exhibit several extrema. The global minimum and maximum consistently correspond to configurations where the inclusion spans the two materials.
- For symmetrical tilt boundaries, energy variations are perfectly symmetric for both dilatational and shear eigenstrains, exhibiting a global minimum located on the interface that decreases with the tilt angle.
- The variations of energy are really significant only within the range  $-1.5R < y_3 < 1.5R$  ( $R$  being the radius of the inclusion and  $y_3$  the position of the inclusion center relative to the interface). Once the inclusion belongs to a same material, the decrease of the imaginary term probably follows the same scaling of  $\left(\frac{R}{y_3}\right)^3$  (cf. Eq. 23) as the imaginary term in an isotropic half-space (Bacon, 1972; Seo and Mura, 1979; Mura, 1987).
- The significance of the image effect related to the described energy variations is quantitatively assessed from comparisons with the interaction energy between a dilatational eigenstrain ( $\varepsilon_{ij}^* = \delta^* \delta_{ij}$ ) and an external stress field (Eq. 28). The image effect remains almost insignificant for the symmetrical tilt boundaries studied but can be comparable to typical interaction energy values for the other orientations considered (cf. Table 1). Moreover, the bigger the dilatation of the inclusion, the higher the

probability that the image effect is significant due to the different scaling (respectively, as  $\delta^{*2}$  for the image effect and as  $\delta^*$  for the interaction energy with a stress field).

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## Appendix A. Full-space Green tensor

The full-space anisotropic Green tensor can be computed as (Barnett, 1972; Lazar, 2016)

$$G_{ij}^\infty(\mathbf{x}, \mathbf{y}) = \frac{1}{8\pi^2|\mathbf{x} - \mathbf{y}|} \int_0^{2\pi} (nCn)_{ij}^{-1} d\phi \quad (\text{A.1})$$

where  $\mathbf{n}$  is a unit-vector perpendicular to  $\mathbf{x} - \mathbf{y}$  and  $(nCn)_{ij} = n_k C_{ikjl} n_l$ .

### Appendix A.1. First derivative of the full-space Green tensor

The first derivative of the full-space anisotropic Green tensor can be evaluated as (Barnett, 1972; Lazar, 2016)

$$\frac{\partial G_{ij}^\infty}{\partial x_k}(\mathbf{x}, \mathbf{y}) = -\frac{1}{8\pi^2|\mathbf{x} - \mathbf{y}|^2} \int_0^{2\pi} \left( \tau_k (nCn)_{ij}^{-1} - n_k F_{ij} \right) d\phi \quad (\text{A.2})$$

where  $\boldsymbol{\tau} = \frac{\mathbf{x} - \mathbf{y}}{|\mathbf{x} - \mathbf{y}|}$  is a unit-vector and  $F_{ij} = (nCn)_{ip}^{-1} \left[ (nC\boldsymbol{\tau})_{pq} + (\boldsymbol{\tau}Cn)_{pq} \right] (nCn)_{qj}^{-1}$ .

### Appendix A.2. Second derivative of the full-space Green tensor

The second derivative of the full-space anisotropic Green tensor can be obtained as the sum of a singular term and a  $\frac{1}{|\mathbf{x} - \mathbf{y}|^3}$  term (Kröner, 1990; Lazar, 2016)

$$\frac{\partial G_{ij}^\infty}{\partial x_k \partial x_m}(\mathbf{x}, \mathbf{y}) = -\delta(\mathbf{x} - \mathbf{y}) E_{ijkm} + \frac{1}{|\mathbf{x} - \mathbf{y}|^3} H_{ijkm} \quad (\text{A.3})$$

The tensor  $\mathbf{E}$  is given as (Lazar, 2016)

$$E_{ijklm} = \frac{1}{4\pi} \int_0^\pi \int_0^{2\pi} n_m n_k (nCn)_{ij}^{-1} \sin \theta d\theta d\phi \quad (\text{A.4})$$

where  $\mathbf{n}$  is here the external unit normal of the unit sphere, i.e.  $n = [\sin \theta \cos \phi, \sin \theta \sin \phi, \cos \theta]$ . The tensor  $\mathbf{H}$  is not needed for the present work. Its expression can be found in (Barnett, 1972; Lazar, 2016).

## Appendix B. Imaginary part of the anisotropic bi-material Green tensor

The purpose of this appendix is to explain briefly the general approach of Pan and Yuan (2000) to obtain the anisotropic elastic Green tensor in a bi-material and to provide the equations needed to perform the numerical calculations. All the details can be found in (Pan and Yuan, 2000).

A full-space bi-material is considered where the region  $x_3 > 0$  is occupied by material (1) and the region  $x_3 < 0$  by material (2). A point force is applied at  $(y_1, y_2, y_3)$ . To find the displacement vector  $\mathbf{u}$  and thus the Green function tensor  $\mathbf{G}^{\mathbf{B}^i}$ , a two-dimensional Fourier transform is applied

$$\tilde{u}_k(\xi_1, \xi_2, x_3) = \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} u_k(x_1, x_2, x_3) e^{i(x_1 \xi_1 + x_2 \xi_2)} dx_1 dx_2 \quad (\text{B.1})$$

In the Fourier transformed domain and in the absence of body force, the equilibrium equation then writes in each material

$$C_{i\alpha k\beta} \xi_\alpha \xi_\beta \tilde{u}_k + i(C_{i\alpha k3} + C_{i3k\alpha}) \xi_\alpha \tilde{u}_{k,3} - C_{i3k3} \tilde{u}_{k,33} = 0 \quad (\text{B.2})$$

where  $\alpha, \beta = 1, 2$ . Writing  $\boldsymbol{\xi} = [\xi_1, \xi_2, 0] = \eta \mathbf{n}$ , a general solution of Eq. B.2 can be expressed as

$$\tilde{u}_k(\xi_1, \xi_2, x_3) = \mathbf{a} \exp(-ip\eta x_3) \quad (\text{B.3})$$

where  $p$  and  $\mathbf{a}$  satisfy the Stroh eigenrelation (Stroh, 1958, 1962) for the oblique plane spanned by  $\mathbf{n} = [\cos \theta, \sin \theta, 0]^T$  and  $\mathbf{m} = [0, 0, 1]^T$

$$[\mathbf{Q} + p(\mathbf{R} + \mathbf{R}^T) + p^2 \mathbf{T}] \mathbf{a} = \mathbf{0} \quad (\text{B.4})$$

whith

$$Q_{ik} = C_{ijks}n_jn_s, R_{ik} = C_{ijks}n_jm_s, T_{ik} = C_{ijks}m_jm_s \quad (\text{B.5})$$

Denoting  $p_i$  and  $\mathbf{a}_i$  ( $i = 1, 2, \dots, 6$ ) the eigenvalues and the associated eigenvectors, respectively, we let

$$\begin{aligned} \text{Im}(p_i) > 0, p_{i+3} = \bar{p}_i, \mathbf{a}_{i+3} = \bar{\mathbf{a}}_i \quad (i = 1, 2, 3) \\ \mathbf{A} = [\mathbf{a}_1, \mathbf{a}_2, \mathbf{a}_3], \mathbf{B} = [\mathbf{b}_1, \mathbf{b}_2, \mathbf{b}_3] \text{ with } \mathbf{b}_i = (\mathbf{R}^T + p_i\mathbf{T}) \mathbf{a}_i \end{aligned} \quad (\text{B.6})$$

where there is no summation over the repeated index  $i$  in Eq. B.6. From a practical perspective, the eigenvalues and the eigenvectors are actually computed from the following standard eigenrelation which is a rewriting of Eqs. B.4 and B.6 (Ting, 1992)

$$\begin{bmatrix} \mathbf{N}_1 & \mathbf{N}_2 \\ \mathbf{N}_3 & \mathbf{N}_1^T \end{bmatrix} \begin{bmatrix} \mathbf{a} \\ \mathbf{b} \end{bmatrix} = p \begin{bmatrix} \mathbf{a} \\ \mathbf{b} \end{bmatrix} \quad (\text{B.7})$$

$$\mathbf{N}_1 = -\mathbf{T}^{-1}\mathbf{R}^T, \mathbf{N}_2 = -\mathbf{T}^{-1}, \mathbf{N}_3 = \mathbf{R}\mathbf{T}^{-1}\mathbf{R}^T - \mathbf{Q} \quad (\text{B.8})$$

Moreover, the eigenvectors are normalized according to the relation (Pan and Yuan, 2000)

$$\mathbf{b}_i^T \mathbf{a}_j + \mathbf{a}_i^T \mathbf{b}_j = \delta_{ij} \quad (\text{B.9})$$

Finally, a useful quantity that will appear in the analysis is the tensor  $\mathbf{M}$  defined by

$$\mathbf{M} = -i\mathbf{B}\mathbf{A}^{-1} \quad (\text{B.10})$$

The general solution in the transformed domain is obtained as the superposition of the six eigensolutions. The unknown quantities are determined from continuity relations at the plane  $x_3 = y_3$  where the point force is applied and from the continuity of the displacement and traction vectors at the interface  $x_3 = 0$  (Pan and Yuan, 2000). Then, the solution in the physical domain,  $\mathbf{G}^{Bi}$ , is derived by applying the inverse Fourier transform in the polar coordinate (Pan and Yuan, 2000). In the present work,  $\mathbf{G}^{Bi}$  is written as the sum of a full-space term and an imaginary term  $\mathbf{G}^{Im}$ . The full-space homogeneous Green tensor is explicitly given by Eq. A.1 but it is noteworthy that it can also be expressed via the present Stroh formalism. The numerical

computation is however a little bit longer due to the fact that an eigenproblem must be solved for each value of  $\theta$  used in the line integral numerical approximation. This observation remains true for the computation of  $\mathbf{G}^{Bi}$ .

The final expressions of  $\mathbf{G}^{Im}$  are finally given below. If  $x_3 > 0$  and  $y_3 \geq 0$ , we have (Pan and Yuan, 2000; Chu et al., 2012)

$$\mathbf{G}^{Im}(\mathbf{x}, \mathbf{y}) = \frac{1}{2\pi^2} \int_0^\pi \overline{\mathbf{A}}_1 \mathbf{G}_u^{(11)} \mathbf{A}_1^T d\theta \quad (\text{B.11})$$

with

$$(G_u^{(11)})_{ij} = \frac{(G_{11})_{ij}}{-\overline{p}_i^{(1)} x_3 + p_j^{(1)} y_3 - (x_1 - y_1) \cos \theta - (x_2 - y_2) \sin \theta} \quad (\text{B.12})$$

$$\mathbf{G}_{11} = -\overline{\mathbf{A}}_1^{-1} (\overline{\mathbf{M}}_1 + \mathbf{M}_2)^{-1} (\mathbf{M}_1 - \mathbf{M}_2) \mathbf{A}_1 \quad (\text{B.13})$$

where  $\mathbf{A}_1$ ,  $\mathbf{M}_1$  and  $p_i^{(1)}$  are obtained by solving the Stroh eigenrelation (Eq. B.7) in material (1), while  $\mathbf{A}_2$ ,  $\mathbf{M}_2$  and  $p_i^{(2)}$  are obtained by solving the Stroh eigenrelation (Eq. B.7) in material (2).

If  $x_3 < 0$  and  $y_3 > 0$ , we have (Pan and Yuan, 2000; Chu et al., 2012)

$$\mathbf{G}^{Im}(\mathbf{x}, \mathbf{y}) = -\frac{1}{2\pi^2} \int_0^\pi \mathbf{A}_2 \mathbf{G}_u^{(21)} \mathbf{A}_1^T d\theta - \mathbf{G}^{\infty 2}(\mathbf{x}, \mathbf{y}) \quad (\text{B.14})$$

$$(G_u^{(21)})_{ij} = \frac{(G_{21})_{ij}}{-\overline{p}_i^{(2)} x_3 + p_j^{(1)} y_3 - (x_1 - y_1) \cos \theta - (x_2 - y_2) \sin \theta} \quad (\text{B.15})$$

$$\mathbf{G}_{21} = \mathbf{A}_2^{-1} (\overline{\mathbf{M}}_1 + \mathbf{M}_2)^{-1} (\mathbf{M}_1 + \overline{\mathbf{M}}_1) \mathbf{A}_1 \quad (\text{B.16})$$

If  $x_3 < 0$  and  $y_3 \leq 0$ , we have (Pan and Yuan, 2000; Chu et al., 2012)

$$\mathbf{G}^{Im}(\mathbf{x}, \mathbf{y}) = -\frac{1}{2\pi^2} \int_0^\pi \mathbf{A}_2 \mathbf{G}_u^{(22)} \overline{\mathbf{A}}_2^T d\theta \quad (\text{B.17})$$

$$(G_u^{(22)})_{ij} = \frac{(G_{22})_{ij}}{-p_i^{(2)} x_3 + \overline{p}_j^{(1)} y_3 - (x_1 - y_1) \cos \theta - (x_2 - y_2) \sin \theta} \quad (\text{B.18})$$

$$\mathbf{G}_{22} = \mathbf{A}_2^{-1} (\overline{\mathbf{M}}_1 + \mathbf{M}_2)^{-1} (\overline{\mathbf{M}}_1 - \overline{\mathbf{M}}_2) \overline{\mathbf{A}}_2 \quad (\text{B.19})$$



If  $x_3 > 0$  and  $y_3 < 0$ , we have (Pan and Yuan, 2000; Chu et al., 2012)

$$\mathbf{G}^{Im}(\mathbf{x}, \mathbf{y}) = \frac{1}{2\pi^2} \int_0^\pi \overline{\mathbf{A}_1} \mathbf{G}_u^{(12)} \overline{\mathbf{A}_2}^T d\theta - \mathbf{G}^{\infty 1}(\mathbf{x}, \mathbf{y}) \quad (\text{B.20})$$

$$(G_u^{(12)})_{ij} = \frac{(G_{12})_{ij}}{-\overline{p}_i^{(1)} x_3 + \overline{p}_j^{(2)} y_3 - (x_1 - y_1) \cos \theta - (x_2 - y_2) \sin \theta} \quad (\text{B.21})$$

$$\mathbf{G}_{12} = \overline{\mathbf{A}_1}^{-1} (\overline{\mathbf{M}_1} + \mathbf{M}_2)^{-1} (\overline{\mathbf{M}_2} + \mathbf{M}_2) \overline{\mathbf{A}_2} \quad (\text{B.22})$$

*Appendix B.1. First derivatives of the imaginary part of the anisotropic bi-material Green tensor*

The first derivatives of  $\mathbf{G}^{Im}$  are obtained by straightforward derivations. Therefore, they are written explicitly only for the case  $x_3 > 0$  and  $y_3 \geq 0$ .

$$\frac{\partial G_{ij}^{Im}}{\partial x_k}(\mathbf{x}, \mathbf{y}) = \frac{1}{2\pi^2} \int_0^\pi \overline{(A_1)_{im}} \frac{\left(\partial G_u^{(11)}\right)_{mn}}{\partial x_k} (A_1^T)_{nj} d\theta \quad (\text{B.23})$$

$$\frac{\partial (G_u^{(11)})_{ij}}{\partial x_1} = \frac{\cos \theta (G_{11})_{ij}}{\left(-\overline{p}_i^{(1)} x_3 + \overline{p}_j^{(1)} y_3 - (x_1 - y_1) \cos \theta - (x_2 - y_2) \sin \theta\right)^2} \quad (\text{B.24})$$

$$\frac{\partial (G_u^{(11)})_{ij}}{\partial x_2} = \frac{\sin \theta (G_{11})_{ij}}{\left(-\overline{p}_i^{(1)} x_3 + \overline{p}_j^{(1)} y_3 - (x_1 - y_1) \cos \theta - (x_2 - y_2) \sin \theta\right)^2} \quad (\text{B.25})$$

$$\frac{\partial (G_u^{(11)})_{ij}}{\partial x_3} = \frac{\overline{p}_i^{(1)} (G_{11})_{ij}}{\left(-\overline{p}_i^{(1)} x_3 + \overline{p}_j^{(1)} y_3 - (x_1 - y_1) \cos \theta - (x_2 - y_2) \sin \theta\right)^2} \quad (\text{B.26})$$

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