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Title: The stroke rate influences performance, technique and core stability during rowing ergometer.

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Abstract:

 The aim of this study was to determine the effect of stroke rate on performance, technique and core stability during rowing ergometer. Twenty-four high-level rowers performed maximal intensity one-minute bouts at 20, 28 and 34 spm on a RowPerfect3 ergometer. Power at the handle, legs, trunk and arms levels were determined and core kinematics and neuromuscular activations were measured. The power at the handle was enhanced with a higher stroke rate in the first half of the drive phase due to higher segment's powers. This resulted in technical changes, as for instance greater mean to peak power ratio at each segment level. The higher trunk power preceded a delayed trunk extension but without significant increase in the erector spinae activation. This underlines the role of the core stability to transfer forces at a higher stroke rate. However, no co-activation parameters between trunk flexors and extensors helped further to understand this force transfer. Rowing at low stroke rate can be a training strategy to work on earlier trunk extension, while maintaining erectors spinae levels of activation. Training at higher stroke rate will induce a rowing technique closer to competition with greater neuromuscular activations, and maximise power production.

 Keywords: Power production - Trunk kinematics - Pelvis kinematics - Neuromuscular control - Muscles co-activations

Introduction

 In rowing, stroke rates can range from 18 strokes per minute (spm) during some training sessions to rates over 40spm during a 2000m race (Hofmijster et al., 2007, 2009; Kleshnev, 22 2016). Moreover, the stroke rate also varies during the race, with for instance values between 34 to 48spm for the M1x finalists at the 2022 World Rowing Championships in Racice in the Czech Republic (Kleshnev, 2022).

 The mean power output at the handle, main performance parameter in ergometer rowing (Bourdin et al., 2004, 2017; Buckeridge et al., 2016B; Colloud et al., 2006; Greene et al., 2013; Kleshnev, 2016) is increased with the stroke rate rise (Buckeridge et al., 2012; Held et al., 2020; Hofmijster et al., 2007; Kleshnev, 1996; McGregor et al., 2004), ranging for example from 254W per cycle at 20spm to 473W per cycle at a competitive stroke rate (Buckeridge et al., 2012). Furthermore, the rowing technique also changes with the stroke rate to allow this increase in power production. Indeed, the stroke rate has an impact on time to peak or mean to peak power (Holt et al., 2020; Kleshnev, 2016; Smith & Draper, 2006; McGregor et al., 2004), lower limb and spine joints kinematics (McGregor et al., 2004; Buckeridge et al., 2016A; Li et al., 2020) or power patterns at the handle, legs, trunk or arms level (Ettema et al., 2022; Kleshnev, 1996). However, given that the stroke rate manipulation modifies the distribution between the drive and the recovery times (Buckeridge et al., 2014; McGregor et al., 2004), these results from the different studies in the literature should be interpreted with caution. Therefore, the effect of the stroke rate on the rowing technique should be analysed on the drive phase only (Ettema et al., 2022).

 With its central position within the kinetic chain from the legs to the arms, the trunk plays a major role in rowing performance. Indeed, the trunk is responsible for about 30% of the handle power (Kleshnev, 2000). With the increase of the stroke rate (ranging from 17 to 36spm), greater spinal forces and larger ranges of motion (ROM) of the pelvis, the lumbar and the thoracic spine angles were noticed (Buckeridge et al., 2016A; Li et al., 2020; McGregor et al., 2004), underlining core stability's adaptations. Core stability refers here to the ability of the trunk, with respect to the pelvis, to produce power and to transfer efficiently forces from lower limbs to the arms (Kibler, Press & Sciascia, 2006). In rowing, the core might act as a power producer (Kleshnev, 2000) and has to efficiently transfer forces from the legs to the arms. With the stroke rate increase, the role of the core in transferring the force could be enhanced as the legs produce more power (Held et al., 2020). However, its function as a power producer could also be greater as its kinematics varies with higher stroke rates. Regarding the neuromuscular aspect of the core, an early activation of spinal and gluteus muscles, followed by a relatively short co-activation phase between abdominals and spinal muscles, and then a late activation of abdominis and external oblique muscles have been described along the drive phase (Pollock et al., 2009). The co-activation between the spinal muscles and the abdominals could lead to an increase in spine stiffness (Cholewicki et al., 1997) and to a better force transfer from the lower limbs to the arms. However, the influence of stroke rate on the core neuromuscular activity remains unknown. A deeper understanding of this relationship could lead to better adaptation of core muscle training. In light of these information, it is plausible that stroke rate manipulation could influence core muscle co-activation together with core stability kinematics, and thus performance.

 The purpose of this study was to determine the effect of the stroke rate on rowing ergometer performance, technique and core stability. We hypothesised that i) the production of power at the handle and at each body segments would be greater through the drive phase for the higher stroke rate condition, ii) the core kinematics would vary through the drive phase inducing a larger ROM for the higher stroke rate condition, iii) the core muscle activity and the amount of co-activation would be larger for the higher stroke rate condition.

Methods

Participants

 Twenty-four rowers with international or national experience were recruited (17 men and 7 72 women; 20.8 ± 2.8 years old; 1.84 ± 0.07 m; 77.6 ± 6.1 kg; 6min $34s \pm 30$ s on 2000 m rowing ergometer performance). Participants who had current low back pain or any injury were not included in the study. The study was approved by the ethics committee Sud-Ouest et Outre Mer III (approval reference 20.07.21.43000-ID_9115) and was conformed to requirements stipulated in the Declaration of Helsinki. All participants were informed about the procedures, purpose and possible risks associated with the experimental set-up and gave their written consent prior to testing.

Test procedure

 After a free warm-up of 10 minutes, each rower performed three one-minute bouts at 20, 28 and 34spm. A trial at their self-chosen optimal stroke rate was performed to normalise EMG signals. The instruction was to row at maximum intensity for each stroke rate.

 The participants rowed on a mobile rowing ergometer (RP3®, Care RowPerfect BV, Haaksbergen, The Netherlands), equipped with custom-made load cells with strain gauges at left and right foot-stretchers and at the pull handle cable (BioRow Tech, BioRow, London, UK), to determine the applied effective forces. Moreover, seat, trunk, and handle displacements were measured using three position sensors (BioRow Tech, BioRow, London, UK) (Figure 1). These data were sampled at 25 Hz.

 Figure 1: Rowing ergometer (RP3) equipped with the BioRow Tech position sensors (A, circled), and force sensors (B for the feet and C for the handle). Both foot force sensors were covered by the usual foot fixation (B, right foot).

 Core stability's sagittal kinematics was recorded with two inertial measurement units (STT- IWS, STT Systems, San Sebastián, Spain) placed in the back at the T6 vertebrae level (between the two scapulae) and between the two posterior superior iliac spines, measuring respectively the movement of the trunk and the pelvis. These two sensors did not cause any discomfort to the athlete, given their small volume (56 x 38 x 18 mm) and low mass (0.046 kg). This system had a static pitch accuracy less than 0.5° around medio-lateral axis and a sampling frequency of 100 Hz.

 Surface electromyography (EMG) recordings of core muscles were obtained from the rectus abdominis (RA), the external obliquus (EO), the erector spinae (ES), the tensor fasciae latae 104 (TF) and the gluteus maximus (GM), bilaterally (TrignoTM Snap Lead wireless sensors, Delsys, Natick, MA, USA). After the skin had been shaved, sanded and cleaned, to ensure an 106 impedance below 5 k Ω , electrodes (Ambu® BlueSensor SP, Ambu A/S, Ballerup, Denmark) were attached parallel to the muscle fibers in line with the SENIAM project's recommendations (Hermens et al., 2000). RA electrodes were placed 2 cm laterally from the umbilicus, EO electrodes at 15 cm laterally from the umbilicus, ES electrodes at about 2 cm of the L1 spinous process, TF electrodes on the line from the anterior spina iliaca superior to the lateral femoral condyle in the proximal 1/6 and GM electrodes were placed at 50% on the line between the sacral vertebrae and the greater trochanter. These EMG signals were sampled at 2000 Hz and synchronised with the motion analysis system.

Data analysis

 Seat, trunk and handle positions as well as foot-stretcher and handle effective forces were 117 filtered with a $4th$ order Butterworth low-pass filter at 5 Hz and 10 Hz, respectively (Fohanno

- et al., 2015; Greene et al., 2009). After the computation of handle, seat and trunk speed from
- their measured position, the power at each level was determined as time-series data as follows (Kleshnev, 2000):
- 121 Phandle (W) = handle force $*$ handle speed.
- 122 Plegs (W) = (left foot-stretcher force + right foot-stretcher force) $*$ seat speed.
- 123 Ptrunk (W) = handle force $*$ (trunk speed seat speed).
- 124 Parms (W) = handle force $*$ (handle speed (trunk speed seat speed)).

 The mean powers were then calculated over the whole drive phase. Time to peak power (T2P, 126 %) from the catch was calculated for each segment as the occurrence of peak power delivery over the normalised drive time. Moreover, the mean to peak power ratio (M2P) was calculated for legs, trunk and arms by dividing the mean power by the peak power. The rationale for M2P was the potential relationship between the power curve shape and performance (i.e. the flatter the better) (Smith & Draper, 2006). The contribution of each segment was computed based on the mean power of the segment divided by the sum of all three segments mean power, multiplied by 100.

133 Trunk and pelvis spatial orientations were filtered with a $4th$ order Butterworth low-pass filter at 10 Hz. Trunk and pelvis catch and finish positions were computed to determine the range of motion (°) of these two body segments. A positive segment angle represented an extension with respect to the vertical axis.

137 The electromyographic signal of each muscle was filtered (Butterworth $4th$ order bandpass filter, 30-450 Hz) and quantified using the root mean square (RMS) value (mV). A 25 ms electromechanical delay was considered (Le Mansec et al., 2019). The EMG signals for the self-chosen rate condition were low pass filtered (6 Hz) to create an envelope. Then, the EMG RMS was normalised against its EMG envelop peak value during the self-chosen rate condition. Left and right RMS normalised values were averaged. In addition, trunk neuromuscular control was further analysed using Directed Co-Contraction Ratio (DCCR) and the Co-Contraction Index (CCI). DCCR (1) was used to represent the balance between trunk agonists and antagonists' muscles activation (Donnelly et al., 2015), while CCI (2) gave an indication about the amount of trunk co-activation (Rudolph et al., 2000). These neuromuscular parameters were computed through the drive phase as follows:

If agonists' mean activation was higher than antagonists' mean activation then:

149
$$
DCCR = 1 - \frac{\overline{EMG}{}_{antagonists}}{\overline{EMG}{}_{agonists}}
$$
 Else:
$$
DCCR = \frac{\overline{EMG}{}_{agonists}}{\overline{EMG}{}_{antagonists}} - 1
$$
 (1)

where the ES were defined as agonists to the movement, and RA and EO were defined as

antagonists. For instance, greater ES

$$
CCI = \frac{Lower \overline{EMG}}{Higher \overline{EMG}} * (Lower \overline{EMG} + Higher \overline{EMG})
$$
 activations induced larger DCCR.
(2)

 where the agonists and antagonists were defined as higher or lower depending on their relative level of activity. For instance, balanced activations between extensor and flexor muscles, combined with greater level of activity induced larger CCI. But either unbalanced activation or lower level of activity decreased the CCI.

 All data were analysed over the drive phase, determined by the handle position. The beginning of this phase, the catch, was defined by the minimum handle position, and the finish by the maximum handle position. Data were analysed using MATLAB software (version 9.2, MathWorks, Inc., Natick, MA, USA).

Statistics

 All power, kinematic and core stability variables were averaged over the middle 12 driving phases for each participant. One subject kinematic data was not usable for analysis, probably because of sweating unsticking the trunk IMU, therefore the kinematic analysis was only conducted on the remaining 23 subjects.

 Data normality was checked by the Shapiro Wilk test, and the alpha level was set at 0.05 (Statistica v10, StatSoft Inc, Tusla, USA). Repeated-measures ANOVAs were used to quantify the effect of stroke rate on the mean power, T2P, M2P, power contribution of each segment, and on pelvis and trunk ROM and angles at catch and finish positions, as well as EMG RMS. Mauchly's test of sphericity was used to check for equality of variance between the three different stroke rates. If the Greenhouse–Geisser epsilon was > 0.75 the Huynh Feldt correction was used, else the Greenhouse Geisser correction value was used (Girden, 1992). The Tuckey post-hoc test was used to test the direction of the effect following the ANOVA and Cohen's d test was then applied to determine the effect sizes between pairs of 178 significantly different variables $(0.2 - 0.5)$ interval for a small effect, $0.5 - 0.8$ for a medium effect and over 0.8 for a large effect).

 Secondly, differences in segments power, kinematics, as well as muscles activations and co- activations, between stroke rates were examined over the drive phase using one-dimensional statistical parametric mapping (SPM) using Random Field Theory (Pataky et al., 2013). SPM repeated measures ANOVA were conducted in MATLAB using the open source spm1d code (spm1d version M.0.4.8; spm1d.org), and then paired t-test SPM were computed on significant variables. After the Bonferroni correction, the alpha significance level for SPM t-tests was set at 0.017.

Results

189 The stroke rates for the three trials were 20.7 spm (± 0.5) , 28.0 spm (± 0.5) , 34.0 spm (± 0.8) . 190 The stroke length was not different between the conditions $(1.67\pm0.12 \text{ m}$ for 20 spm, 1.68±0.11 m for 28 spm, 1.67±0.11 m for 34 spm).

Performance

193 Mean power handle significantly increased with stroke rate, from 939 W (± 236) for 20 spm 194 to 1012 W (\pm 237) and 1060 W (\pm 240) for 28 spm and 34 spm, respectively (Cohen's d $>$ 0.8 for the three comparisons). SPM ANOVA indicated a larger handle power production with the increase of the stroke rate, from 15% to 60% of the drive phase (p<0.05; F=7.421). The power produced at the handle was significantly greater for 28 spm than 20 spm, but only between 16% and 57% of the drive phase. For 34 spm, the power at the handle was larger than 20 spm in the 15-57% window (Figure 2) and greater than 28 spm in the 16-54% window.

202 Figure 2. Group average (mean \pm SD) power production at the handle (W) during the drive phase (%) for the 20 spm (in red) and 34 spm (in blue) conditions. The grey shaded area 204 represents the significant differences time-window $(p < 0.017)$.

Rowing technique

 The mean powers of each segment were significantly greater with stroke rate increase (Table 208 1; $p < 0.001$), with medium to large effect sizes. The segments power contribution was slightly but significantly different with the stroke rate, with a small increase in the legs power contribution at 34spm, while the one at the arms level was lower (Table 1). The 211 corresponding effect size was medium $(0.5 < d < 0.8)$.

212 Table 1. Comparison of the mean \pm SD power (W) and contribution \pm SD (%) at each segment level. Main cadence effect is reported with the p value level or NS (not significant). 214 *Significant difference from 20 spm ($p < 0.05$). ^{\$}Significant difference from 28 spm ($p <$ 0.05).

	Mean power handle	Mean power legs	Legs' contribution	Mean power trunk	Trunk's contribution	Mean power arms	Arms' contribution
	(W)	(W)	(9/0)	(W)	(9)	(W)	(9/0)
	p < 0.001	p < 0.001	p < 0.05	p < 0.001	NS	p < 0.001	p < 0.001
20 spm	939 ± 236	410 ± 105	43.1 ± 3.8	335 ± 106	34.6 ± 4.5	210 ± 61	22.3 ± 4.5
28 spm	$1012 \pm 237*$	$447 \pm 105*$	43.6 ± 3.8	$362 \pm 111*$	34.7 ± 4.3	$221 \pm 60^*$	$21.7 \pm 4.3*$
34 spm	1060 ± 240 *\$	471 ± 105 [*]	$43.8 \pm 3.2^*$	379 ± 111 *\$	34.6 ± 3.9	229 ± 58 *\$	$21.5 \pm 4.1*$

 Rowing technique variables for the handle, the legs, the trunk and the arms are presented in 219 Table 2. Peak power of the legs occurred earlier $(p < 0.01$, medium effect size), while the one 220 for the arms was delayed ($p < 0.001$, small effect size) with the increase of the stroke rate. But the peak power of the handle and the trunk remained unchanged. Moreover, mean to peak power values of the different segments were larger for the higher stroke rate (medium to large effect sizes for the legs and trunk, and large effect size for the arms). The corresponding rowing style, shown in Figure 3, was close to the Rosenberg style, as defined by Kleshnev (2016), with sequencing leg and trunk power production and an important contribution of the trunk power to performance. The power curves and statistical comparison between 20 spm and 34 spm are presented in Figure 4 for the legs, the trunk and the arms. Significant differences in power (SPM ANOVA) were between the beginning and 47% for the legs, within the 27-58% window for the trunk and the 15-34% window for the arms. For the legs, the significant differences time-window were 2-45% between 20 spm and 28 spm and 1-36% between the 28 spm and 34 spm. At the trunk level, differences occurred within 32-57% and 31-49% of the drive phase when comparing 20 spm and 28 spm and 28 spm and 34 spm, respectively. Lastly, the arms power significant differences time-window was 17-29% between 28 spm and both other rates.

235 Table 2. Comparison of mean \pm SD time to peak power (T2P, % of the drive phase) and mean to peak power (M2P) of each segment. Main cadence effect is reported with the p value level 237 or NS (not significant). *Significant difference from 20 spm ($p < 0.05$). s Significant 238 difference from 28 spm $(p < 0.05)$.

241
242 Figure 3. Group average power (W) production at the handle and for each segment, during the drive

phase (%) for the 34 spm condition. All three stroke rates visually depicted similar patterns.

 Figure 4. Group average (mean ± SD) power production of the legs (A), trunk (B) and arms (C) power production (W) during the drive phase (%) for the 20 spm (in red) and 34 spm (in blue) conditions. The

grey shaded area represents the significant differences time-window (p < 0.017).

Core Stability kinematics

 Only the trunk angle at the catch position was significantly influenced by the stroke rate, with a larger forward lean (with a medium effect size) at the higher stroke rate (Table 3). Pelvis angle profiles through the drive phase demonstrated a retroversion but did not differ between the conditions. However, trunk angle profiles differed significantly between all rates (SPM ANOVA p<0.05, in the 0-93% window). The significant differences between 20 spm and 34 spm occurred in the 0-91% window (Figure 5). Differences were also significant between the other rates, but in a lesser extent, i.e. within 49-76% between 20 spm and 28 spm, and within 58-93% between 28 spm and 34 spm. The trunk remained in a flexed position from the beginning to 70-80% of the drive phase and extended then till the end of the drive phase. The higher stroke rate induced a delayed trunk extension starting roughly at 50% of the drive phase, but without impacting the trunk angle at the finish position.

263 Table 3. Comparison of mean \pm SD ranges of motion (ROM, \degree) and angles (\degree) of each segment. Main cadence effect is reported with the p value level or NS (not significant). 265 *Significant difference from 20 spm $(p < 0.05)$.

Pelvis ROM $(°)$	Trunk ROM $(°)$	Pelvis catch position $(°)$	Trunk catch position $(°)$	Pelvis finish position $(°)$	Trunk finish position $(°)$
NS	NS	NS	p < 0.001	NS	NS
42.4 ± 7.5	74.9 ± 8.8	-0.4 ± 9.9	-55.8 ± 7.1	40.5 ± 12.0	18.0 ± 7.2
42.5 ± 8.1	75.8 ± 8.1	0.1 ± 10.2	$-56.6 \pm 7.2*$	41.2 ± 11.3	18.4 ± 7.2
42.4 ± 7.2	74.9 ± 6.5	0.7 ± 10.4	$-57.2 \pm 7.2^*$	41.5 ± 10.9	17.2 ± 7.4

269 Figure 5. Group average (mean \pm SD) trunk angle (\degree) during the drive phase (%) for the 20 spm (in red) and 34 spm (in blue) conditions. The grey shaded area represents the significant 271 differences time-window $(p < 0.017)$.

Core Stability neuromuscular control

 All muscles had a greater activation with the stroke rate increase, especially at 34 spm, except the ES (Table 4 and Figure 6). The effect sizes for RA were medium, and medium to large for EO, TF and GM muscles. This was true whatever the variable considered (EMG 277 quantification or EMG profile) over the whole drive phase (SPM ANOVA p-values <0.05). In addition, RA were more activated during 60% to 100% of the drive phase for the 28 spm condition compared to 20 spm, and during 64% to 87% for the 34 spm condition with respect to 28 spm. For EO, the significant time-window where differences occurred was between 78% and 100% when comparing 20 spm and 28 spm. In the 34 spm condition, a larger activation was found within 75-100% of the drive phase compared to 28 spm. TF activation differences started at 59% and 64% until the end of the drive phase, for comparison between 20 spm and 28 spm and between 28 spm and 34 spm, respectively. For GM, a significant larger activation was noticed in the early phase (0-16%) for 28 spm compared to 20 spm, whereas no difference was noted between 28 spm and 34 spm.

287 Table 4. Comparison of mean \pm SD of EMG activations (%MVC) of the rectus abdominis (RA) muscles, the external oblique (OE) muscles, the erector spinae (ES) muscles, the tensor of the fascia lata (TF) and the gluteus maximus (GM) muscles. Main cadence effect is reported with the p value level or NS (not significant). *Significant difference from 20 spm (p \leq 0.05). ^{\$}Significant difference from 28 spm (p < 0.05).

294
295 $\overline{P_{\text{0}}^{9}$ = $\overline{P_{\text{0}}}$ = $\overline{P_{\text{$ 296 activations (%MVC) during the drive phase (%) for the 20 spm (in red) and 34 spm (in blue)

297 conditions. The grey shaded area represents the significant differences time-window ($p <$ 0.017).

 No difference in DCCR or CCI was observed. Their patterns are presented in Figure 7. The DCCR presented a larger activation of the trunk extensor muscles than the abdominal muscles within the first 35% of the drive phase. Then, the decrease in this value indicated a transition towards a more abdominal orientated ratio, these muscles becoming the most activated for the remaining 30% of the drive phase. The CCI remained relatively low and stable across the drive phase. For example, if both extensor and flexor groups would have activated in average at 40% of their MVC, then the CCI value would have been 80. The CCI value around 10 in the first and last part of the drive phase are due to the large imbalance between the agonists and the antagonists, despite a large amount of muscles activation. During the central part of the drive phase, the more balanced activation between these muscles is impaired by a rather small amount of activation, maintaining the CCI value low.

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Discussion and Implications

 The present study's aims were to determine the effect of stroke rate on rowing ergometer performance, technique and core stability. The main findings were that i) the power at the handle and at each segment level are enhanced at a higher stroke rate, mostly during the first half of the drive phase, indicating that rowing technique is modified, ii) trunk extension was delayed during the drive phase, without altering its range of motion, and iii) some core muscles showed a greater activation without any change in the co-activation along with the stroke rate increase.

Rowing performance and technique

 Mean powers of handle and segments were largely impacted by the stroke rate variation, showing greater power at higher stroke rate as previously reported in the literature at the handle level (Buckeridge et al., 2012; Held et al., 2020; Hofmijster et al., 2007; Kleshnev, 1996; McGregor et al., 2004), legs level (Held et al., 2020) and every segment level (Kleshnev, 1996). The relative contributions of each segment to the total power (in %) were close to those reported by Kleshnev (2000). Although these contributions were influenced by the stroke rate, the variation remained below 1% and should not be considered as a substantial modification of the segments contribution. The greater handle power at higher stroke rate occurred roughly between 15% and 55% of the drive phase, and is likely to be explained by the increase in legs, trunk and arm power. Indeed, legs and trunk powers were impacted by the stroke rate during the largest part of their power production until their peak power delivery. Consequently, legs time to peak power occurred earlier, while the trunk time to peak power remained unchanged. Although these timing results were different from Kleshnev (1996), one should keep in mind that these power profiles, and hence their sensitivity to stroke rate manipulation, are strongly related to the technical styles, depending on the rower's

 level (Buckeridge et al., 2012; Cerne et al., 2013) and probably on training background (Hill, 2002; Kleshnev, 2016; Warmenhoven et al., 2018B). Surprisingly, although differences in arms power were also observed at a higher stroke rate, these took place only at the beginning of the drive phase too, where only 50% of their maximal power is produced. But arms time to peak power was not in line with this power profile alteration, as it occurred later with the stroke rate increase. This shows the importance of this early phase of the drive to enhance performance through a faster rowing movement. During this phase, rowers might have to provide more power at their arms level to tense the ergometer chain following a faster start at a higher stroke rate. The lack of power profiles difference in the second half of the drive phase, especially at the arms level would explain the comparable handle power production during the last 40%, despite a higher stroke rate. This power alteration resulted in a greater mean to peak power ratio at each level, showing a greater average power relative to the peak power at higher stroke rate. These more "rectangular" or "flattened" curves could be related to greater power output, as observed for elite vs. sub-elite rowers (Smith & Draper, 2006). Therefore, in order to improve their performance at each stroke rate, it is advised to produce a high power at each segment level over the longest portion possible over the drive phase. Moreover, given that stroke rate influences the distribution between the drive and the recovery times, it is recommended to analyze technical and biomechanical variables, in particular time-dependent variables (such as time to peak), over the drive phase only. Furthermore, the rowing technical style, defined in Figure 3, remained unchanged with the stroke rate and close to the Rosenberg style (Kleshnev, 2016). The results presented in this study might not be generalizable to other rowing styles, so future research should consider this in order to better understand the stroke rate effect with respect to the rowing style. Other factors could modify the effect of the stroke rate on the rowing technique as sex (Attenborough et al., 2012; Ng et al., 2013), boat-side (Warmenhoven et al., 2018A), or expertise (Buckeridge et al., 2012). Therefore, larger sample size would be needed to investigate further these potential covariates effects.

Core Stability

 The significant contribution of the trunk to power production with this technical style, i.e. over 30%, highlights the importance of a core stability analysis to better understand its adaptation to the stroke rate. Contrarily to our hypothesis, the trunk and pelvis ranges of motion were not larger for the higher stroke rate, whereas Li et al. (2020) found that the thoracic range of motion was increased between a 18 spm and a 32 spm rowing condition (e.g. by 3.9°). Moreover, the average trunk range of motion in their study, whatever the condition, was around 40°, while ours rather reached 75°. These differences may be the consequence of a different rowing style, and/or the trunk kinematic model. Indeed, the IMU sensor position at the second thoracic vertebrae level in Li et al.'s study (2020), could have been sensitive to a forward roll of the shoulder during rowing, thus reducing the trunk range of motion. In addition, the main difference between our setups was the instruction given to the rowers, as these authors asked for a long training session intensity (i.e. relatively low), whereas rowers had to perform their strokes at maximal intensity in the current study. As this rowing intensity has an impact on lower limb joint powers (Ettema et al., 2022), it is likely that this could influence trunk kinetics and kinematics. These different points could explain the different effect of stroke rate on trunk kinematics between the present investigation and Li et al.'s study (2020). As a large trunk range of motion (with respect to the pelvis) has been linked to better rowing performance (Buckeridge et al., 2016A), we could hypothesise that the large values measured in the present study underline that the trunk range of motion already levelled off to produce the highest performance, given the maximal intensity instruction, and regardless of the stroke rate. The same suggestion could be made for the pelvis kinematics, as

 it remained at the same level, contrarily to previous studies (McGregor et al., 2004; Li et al., 2020). However, the aforementioned studies used a fixed rowing ergometer, which enables pelvic kinematics alterations with the stroke rate, whereas free-floating ergometers don't (Hislop et al., 2010). Interestingly, the gluteus maximus had a greater activation in the early part of the drive phase, while the pelvis kinematics didn't differ. Thus, as the stroke rate rises, their role might be to increase the leg power production by extending the hip, rather than to support further the pelvis retroversion.

 Despite the absence of difference in the trunk range of motion, we observed a delayed extension of the trunk at the higher stroke rate. This delay occurred mostly from 50% to 90% of the drive phase, so after the trunk power significant increase, which ended up around 55%. As erector spinae muscles did not present a larger activation and trunk extension was delayed, this indicates that the larger trunk power would not be the consequence of a trunk-located mechanism of power production, but probably because of a transfer from the lower limb kinetics. Therefore, when the stroke rate rises, it is possible that the trunk might act more as a force transferrer than a force producer. Other mechanisms should be investigated to enhance our understanding of this force transfer, as for instance the role of passive structures (e.g. thoracolumbar fasciae), intra-abdominal pressure or deeper core muscles (e.g. transversus abdominis). Besides, given that the trunk remained in a flexed position during this force transfer phase, the erector spinae activation level measured in this study might have already been sufficient to support this force transfer, whatever the stroke rate.

 Also, no trunk co-activation strategy has been noticed in the present study, neither with DCCR nor with CCI. Indeed, as depicted in the Figure 7, a clear transition between erector spinae activations and abdominal muscles activations in the middle of the drive phase, combined to the absence of any CCI rise during the 40-60% window of the drive phase, revealed that the co-activation measurements could not help the understanding of force

 transfer mechanisms through the core during ergometer rowing. A high-level of co-activations between abdominals and spine erectors is therefore not required, whatever the stroke rate.

 The statistical parametric mapping analysis also underlined the larger abdominal activations in the late part of the drive phase, that acted eccentrically to control the trunk delayed extension (Pollock et al., 2009). Simultaneously, the larger tensor fasciae latae activation probably helped maintaining pelvic retroversion's stability. All these muscles activities also enabled to anticipate the recovery phase where a trunk flexion and a pelvic anteversion would be required. With the increased stroke rate, core muscles larger activations might reduce the recovery phase duration to perform the demanded stroke rate (Li et al., 2020). As more abdominal and tensor fasciae latae forces might be necessary as the stroke rate rises, we could therefore advice to target eccentric abdominal training for rowers.

Summarizing conclusion

 Our results show that ergometer rowing at a higher stroke rate induces greater power production at the handle and at each body segment during the first half of the drive phase, as well as adaptations in the rowing technique.

 Stroke rate also influences core stability, as illustrated by the delayed trunk extension, controlled by the eccentric action of the abdominal muscles. The core might further act as a force transferrer with the higher stroke rate, despite any increase in the co-activation strategy.

 Rowing at a higher stroke rate certainly places the rower closer to the technical and neuromuscular conditions encountered during a competition, but rowing at a lower stroke rate could be helpful to work on an earlier trunk extension technique, while maintaining erectors spinae levels of activation. Moreover, to improve the force transfer capacity through the core, training at higher stroke rate should be more efficient. Further work is needed to better understand force transfer mechanisms through the trunk during rowing tasks.

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